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**A HYDROSTATICALLY CONSISTENT NORTH AMERICAN
RADIOSONDE DATA BASE AT THE FORECAST
SYSTEMS LABORATORY, 1946-PRESENT**

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CONTENTS

ABSTRACT	1
1. INTRODUCTION	1
2. A COMPARISON OF GTS AND NCDC DATA	3
2.1. Significant-Level Information	4
2.2. Wind Data	5
2.3. Tropopause Data	6
2.4. Mandatory-Level Heights Below the Surface	6
2.5. General Differences	6
3. THE FSL DATA BASE	7
3.1. General Description	7
3.2. Merging Originally Transmitted Wind Information	8
3.3. Reclaiming and Estimating Tropopause Pressure	9
3.4. Adding Heights of Mandatory Pressure Levels Below the Surface	9
4. OBJECTIVE HYDROSTATIC CHECKING AND CORRECTING	11
4.1. Review of Basic Principles and Methodology	12
4.2. Delta (Δ) Calibration	13
4.3. Hydrostatic Checking Procedures	14
4.3.1. Correcting Heights and Temperatures for Two Consecutive Large Deltas	15
4.3.2. Correcting an Isolated Error	16
4.3.3. Uncorrectable Errors: Three or More Consecutive Large Deltas	17
4.4. Enhancements	17
4.4.1. Checking for Superadiabatic Lapse Rates	18
4.4.2. Applying a Pressure-Weighted Log-Average Temperature Calculation	18
4.4.3. Correcting Significant-Level and Wind-Level Data	19
5. APPLYING HYDROSTATIC CHECKING PROCEDURES	19
5.1. Correcting a Sounding With a Simple Height or Temperature Error	19
5.2. Correcting a Sounding With a Simultaneous Height and Temperature Error	20
5.3. Recalculating the Pressure Weighted, Log-Averaged Mean Layer Temperature	20
5.4. Correcting a Sounding With an Isolated Inconsistent Layer	21
5.5. Uncorrectable Errors	21
6. GROSS ERROR CHECKS	22
6.1. Point Data Checks	22
6.2. Data Line Checks	23
6.3. General Sounding Checks	23

CONTENTS (continued)

7.	DIRECT ACCESS DATA RETRIEVAL	23
8.	DATA INVENTORIES AND PROCESSING STATISTICS	25
8.1.	Inventories	25
8.2.	Processing Statistics	25
9.	STATION HISTORICAL DOCUMENTATION	26
9.1.	Basic Station Historical Information	28
9.2.	Equipment Historical Information	29
10.	CONCLUDING REMARKS	29
11.	REFERENCES	30
APPENDIX A	FSL Rawinsonde Data Format	54
APPENDIX B (1)	Record Inventory for North American Upper-Air Stations	55
APPENDIX B (2)	Station History for North American Upper-Air Stations	59
APPENDIX B (3)	Station Equipment History for North American Upper-Air Stations	74
APPENDIX C	Example of the Hydrostatic Checking and Correction Computer Procedure	81

TABLES

Table 1.	GTS rawinsonde report from 0000 UTC, 1 August 1986, for Denver, Colorado	31
Table 2.	NSSFC decoded GTS rawinsonde report from 0000 UTC, 1 August 1986 for Denver, Colorado	32
Table 3.	NCDC archive radiosonde data from 0000 UTC, 1 August 1986, for Denver, Colorado	33
Table 4.	Empirical constant used by the National Weather Service to compute height of mandatory pressure surface below the elevation of a station	34
Table 5.	Value of the coefficient (C_0), proportional to the difference of the log of bounding mandatory pressure levels, used in Equation 4.5	34
Table 6.	Distribution of allowable discrepancies (deltas) for layers bounded by the indicated mandatory levels.	35
Table 7.	Absolute value of allowable discrepancies (deltas) for each mandatory layer (from Rubstov and adapted by Inman, 1968).....	35
Table 8.	Decoded GTS rawinsonde report from 1200 UTC, 2 May 1990, for Chihuahua, Mexico (WMO station 76225), depicting a simple temperature error at 300 mb.	36
Table 9.	Decoded GTS rawinsonde report from 1200 UTC, 2 January 1984, for Quillayute, Washington shown before and after (bottom) hydrostatic correction to the height at 850 mb.	37
Table 10.	Decoded GTS rawinsonde report from 0000 UTC 21 June 1990 for Huntington, West Virginia, shown before (top) and after (bottom) hydrostatic correction to both the height and temperature at 400 mb	38
Table 11.	Decoded GTS rawinsonde report from 0000 UTC, 1 January 1984, for Fort Nelson, B.C., Canada (see Fig. 2), illustrating the effect of a strong temperature inversion on the calculation of the surface layer (966-850 mb) delta..	39
Table 12.	Decoded GTS rawinsonde report from 1200 UTC, 1 January 1984, for Washington, D.C. (see Fig. 3) illustrating the effect of a nonlinear temperature distribution upon the calculation of the 00-500 mb delta.....	40
Table 13.	Decoded GTS rawinsonde report from 0000 UTC, 4 March 1981, for Monett, Missouri, depicting an isolated inconsistent layer at 500 mb.	41

TABLES (continued)

Table 14.	Decoded GTS rawinsonde report from 0000 UTC, 20 January 1984, for Guaymas, Mexico (see Fig. 4) depicting a superadiabatic layer between 1000 and 850 mb.	42
Table 15.	Decoded GTS rawinsonde report from 0000 UTC, 1 January 1981, for Fort Nelson, B.C., Canada, illustrating three consecutive large deltas for which no hydrostatic correction could be applied	42
Table 16.	Gross out-of-range point error checks performed by FSL for processing radiosonde data	43
Table 17.	Segment of the period of record inventory.	43
Table 18.	Example from the full radiosonde inventory file	44
Table 19.	General FSL radiosonde data base statistics.	45
Table 20.	FSL radiosonde data base statistics showing sounding completeness and hydrostatic quality	46
Table 21.	Description of the FSL radiosonde station historical file	47
Table 22.	Description of the FSL radiosonde equipment historical file	48

FIGURES

Figure 1. Comparison of GTS and NCDC-processed wind speed versus Pressure for the Oklahoma City, OK, sounding taken on 11 May 1985.	49
Figure 2. Skew-T, log-P plot of the sounding taken at Fort Nelson, British Columbia, Canada, on 1 January 1984.	50
Figure 3. Same as Fig. 2, except for Washington, D.C. (Dulles).	51
Figure 4. Same as Fig. 2, except for Guaymas, Mexico, on 20 January 1984.	52
Figure 5. File structure for the FSL radiosonde data set.	53

A HYDROSTATICALLY CONSISTENT NORTH AMERICAN RADIOSONDE DATA BASE AT THE FORECAST SYSTEMS LABORATORY, 1946-PRESENT

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ABSTRACT. A data base containing all known upper-air reports for North America has been created at the Forecast Systems Laboratory (FSL). Rawinsonde data acquired from various sources for the period from 1946 to the present were subjected to gross error and hydrostatic consistency checks. The data base was created for two reasons: to satisfy a requirement to support ongoing case studies and climatological research with a conveniently accessible data base located at FSL, and to include data not contained in the data base residing at the National Climatic Data Center (NCDC). This Technical Memorandum describes the creation of the FSL data base and the quality control procedures used. It also includes the methods used to replace parts of the soundings that are missing from the NCDC data, a description of the data access routine, real-time updates to the data base, and station history and inventory information.

1. INTRODUCTION

Vertical distributions of temperature, humidity, and winds are fundamental meteorological observations used in weather forecasting and research. These data are acquired by an instrument known as the radiosonde (or rawinsonde; these terms are used interchangeably in this document), which is sent airborne on weather balloons. Although the radiosonde may eventually be replaced by remote sensing systems, such as the profiler and satellites, it is the benchmark standard for new upper-air observing technologies. Realizing the importance of these data, most governments around the world participate in upper-air observing programs. In North America, the United States has operated a radiosonde observational program continuously since 1937. Observations that are taken by the National Weather Service (NWS) and the U.S. military have extended over the continental United States, Alaska, Hawaii, Canada, Mexico, and the Caribbean.

Upper-air data have been summarized by various methods and published in many places. From 1937 to 1945, statistics were customarily presented for data at constant height intervals above sea level. In 1946, governments around the world converted to a system of measuring upper-air parameters at constant pressure surfaces. The altitudes (heights) of these pressure surfaces are computed and included with the basic observations. Data taken by observation sites under U.S. control have been archived at the National Climatic Data Center (NCDC) in Asheville, North Carolina, since the change to constant pressure in 1946. The NCDC digitizes and performs limited quality control procedures on most original

station records of radiosonde observations. These digitized observations are available on magnetic tape (TD6201 series data) approximately 1 year after the original station records are received for processing at NCDC. The TD6201 digital rawinsonde data base contains most observations taken within North America from 1946 to 1970, but it is missing Canadian and selected U.S. military observations taken after approximately 1970. The data base contains no observations from Canada after 1970 because the control of these stations went to the Canadian government. Canadian data are archived and digitized by the Atmospheric Environment Service (AES) in Downsview, Ontario, and are also available at the National Center For Atmospheric Research (NCAR) in Boulder, Colorado. For reasons unknown at the time of this writing, data from most U.S. military locations are no longer archived in TD6201, nor are they digitized by the military. Therefore, to obtain a complete digital archive of historical and real-time rawinsonde data for North America, one must supplement TD6201 data with data from other sources.

Most stations with a regular radiosonde observing program communicate their observations to national meteorological centers around the world over the Global Telecommunication System (GTS). A GTS radiosonde report is a subset of the original station observation that is coded for international dissemination in accordance with World Meteorological Organization (WMO) regulations. GTS data are recorded on magnetic tape by the National Meteorological Center (NMC) in the United States.

There are significant differences between GTS data and NCDC digital data. Each has desirable and undesirable characteristics for use in a research data base. Using either alone in creating an archive for research is undesirable for several reasons. Since NCDC does not receive all observations, digital Canadian data after approximately 1970 must be obtained from the AES or NCAR, and digital military data for certain locations are available only over GTS. NCDC does not include some of the information available in the GTS message, and NCDC data are not available in near or real time. GTS data are not quality controlled, must be decoded, require that users compute the heights of significant pressure levels and the pressures of winds reported at heights defined by the WMO, are of lower resolution, and are more difficult to access than NCDC data.

Realizing the important differences in the availability, quality control, information content, and ease of access of both data sets, FSL decided to create its own radiosonde data base by merging GTS data with NCDC TD6201 data. In addition to providing rawinsonde data for real-time update capability and data from certain military stations that are no longer digitized and archived at NCDC, archived GTS data contain originally transmitted winds, maximum wind, and original tropopause information. Since 1971 NCAR has provided FSL with NCDC TD6201 data and Canadian data. Although GTS data have been available from NCAR, NCDC, and other research organizations since 1960, they are difficult to access because

other globally transmitted meteorological data (e.g., surface observations) are usually stored along with the radiosonde data. Fortunately, FSL was able to acquire an easily accessible archive of GTS radiosonde data for 1970 to 1985 from the National Severe Storms Forecast Center (NSSFC). In 1986, FSL began a real-time decoding and archiving system for GTS data, and no longer needs to go outside the laboratory for them.

In this document we discuss how the FSL data base was created, what it contains, what additional quality control procedures are used, and how the data can be accessed. Section 2 discusses the differences between GTS and NCDC radiosonde data. Section 3 describes the principal components of the FSL merged data set, and how the NCDC and GTS data were merged. Section 4 covers the hydrostatic checking and correction procedure that is applied to all the data. The technique is similar to the one previously employed by Inman (1968) at the National Severe Storms Laboratory but is more sophisticated in its application. Examples applying this technique to erroneous data are presented in Section 5. In Section 6, other diagnostic gross error handling procedures are discussed. In Section 7, the data storage and access methods are briefly outlined. It is the ease and flexibility of accessing the FSL data base that distinguishes it from other, similar data bases available elsewhere. Section 8 discusses the data inventories FSL has created. These digitally available inventories provide the researcher a convenient way of determining the availability of data. In Section 9 we describe our effort to establish a digital upper-air station historical file.

Appendix A contains a legend for interpreting the FSL data base format. The user will want to refer to this appendix since the data examples in Sections 2 and 5 use this format. Appendix B (1) lists a period of record inventory, Appendix B (2) gives the station history, and Appendix B (3) gives the station equipment history. To use historical radiosonde data intelligently requires knowledge of station location, elevation, instrumentation, and identification numbers. Before we processed the data and created a station history, there had not been a digital station history for upper air at NCDC. This version of the history is now available at the NCDC. Appendix C shows an example of the hydrostatic checking and correction computer procedure for those interested in software. (The complete code can be obtained. See Appendix C for more information.)

2. A COMPARISON OF GTS AND NCDC DATA

Table 1 contains a typical sounding in its GTS format up to 100 mb that can be decoded using the Federal Meteorological Handbook No 4 (U.S. Departments of Commerce, Defense, and Transportation, 1976). Tables 2 and 3 show the same sounding data decoded and put into the FSL format (see Appendix A), but from

NSSFC and after NCDC processing, respectively. NSSFC decodes the GTS message and computes the heights of significant levels and the pressures of wind levels. Comparing Table 1 or 2 with Table 3 reveals important differences between GTS data and data after processing at the NCDC. These are reviewed below.

2.1. Significant Level Information

There are two reasons why the NCDC data have more significant levels (identifier, first column in Table 3) than the GTS data. First, the NCDC data base has significant-level information at every 50 mb increment, and at 25 mb increments above 200 mb because of a decision to generate this information to satisfy a climatological requirement for 50-mb and 25-mb data. Although there is no documentation on how these levels are computed, we determined that logarithmic interpolation in pressure ($\log p$) is performed to compute the temperature at these levels using the nearest originally measured significant-level or mandatory-level temperatures. The temperature at pressure level n , T_n , is computed from T_h and T_l , the temperature at pressure level P_h and pressure level P_l , according to the following formula:

$$T_n = T_l + (T_h - T_l) \ln(P_n/P_l) / \ln(P_h/P_l). \quad (2.1)$$

For example, from Table 3, we can confirm that the temperature at 800 mb is 22.3°C by using the temperatures at 833 and 700 mb, 25.4°C and 12.1°C, respectively, in Eq. 2.1. The computed 800 mb height (2051 m) can be obtained by using the hydrostatic equation (described in Section 4) between 833 and 800 mb by employing the temperature at 800 and 833 mb and the height at 833 mb. When there is more than one level to which data are to be interpolated (e.g., given observed data at 833 and 700 mb, NCDC will generate data at 800 and 750 mb), only observed data are used to generate other data (i.e., the 800 mb interpolated data are not used to generate the 750 mb data). For data before 1976, it is impossible to distinguish generated data from real data in the NCDC data base. However, since 1976 generated data are flagged.¹

The second reason for additional significant-level information in the NCDC data is that NCDC archives high-resolution data recorded at the actual upper-air sites, in accordance with the criteria for selection of significant level outlined in the Federal Meteorological Handbook No. 3 (U.S. Department of Commerce et al., 1981): "At pressures of 300 mb or greater, or the first conventional

¹Since we acquired the majority of our data from NCAR, where the latest NCDC TD-6201 series data was not received until 1984, none of our data contains the generated data flag. However, as time permits, future updates of our data base will include these flags indicating generated data levels.

tropopause, whichever is reached first, the temperature at any level between two adjacent significant levels should not differ by more than 0.5°C from that obtained by linear interpolation between the two selected levels." Significant levels for the GTS coded messages, however, are selected in accordance with the WMO reporting criteria, which use a departure from linearity of 1.0°C. Criteria differ for data above 300 mb and for relative humidity. The departure from linearity for temperature data above 300 mb is 2°C and 1°C for GTS and NCDC data, respectively. For relative humidity selection, a 10% departure from linearity is applied to GTS data and 5% is applied to NCDC data. The sample sounding in Table 3 shows, in addition to the generated 50 mb data, levels at 595, 554, 321, 175, 174, 142, 122, and 113 mb, which were not included in the GTS data because of the difference in the application of the significant criteria.

NCDC data from before 1970 often contain only generated significant-level information at 50 mb increments up to 200 mb and 25 mb increments up to 100 mb. The actual significant levels used to generate that information, along with original station records, are no longer available. This is an unfortunate situation for the researcher expecting to obtain a full thermodynamic profile of the atmosphere from the archive prior to 1970.

2.2. Wind Data

The NCDC report in Table 3 contains winds at the thermodynamically significant levels. In the original GTS data (Table 1), winds are coded for WMO transmission at "regionally fixed and significant" (PPBB) levels. At NCDC, the winds are received from the observation sites at 1-min balloon ascent intervals (these data are not available in digital form, but they are available on microfilm). These 1-min winds are then interpolated to the thermodynamically significant levels. Figure 1 is an example of the distributions of wind speed with height for the PPBB section of the GTS report and the NCDC interpolated data for the 0000 UTC 11 May 1985 sounding at Oklahoma City, Oklahoma. The interpolation smooths some of the information contained in the original GTS wind profile. In addition, there are small differences in the mean wind and maximum wind speeds between the two data sources. We compared mean and maximum winds for GTS and NCDC thermodynamic-level winds for approximately 4 days from June 1982 (approximately 600 soundings). Wind speed differences greater than 0.5 knots occurred 63% of the time. Differences greater than 5 knots occurred in 10 soundings.

Interpolating the 1-min wind data to the significant levels makes the number and location of wind levels in the NCDC soundings a function of the number and location of thermodynamically significant levels. Significant wind levels could be omitted if they do not fall near a thermodynamically significant

level. Likewise, unnecessary attention may be given to the wind profile if many thermodynamically significant levels fall close to one another.

The original transmission of mandatory-level data (TTAA section of Table 1; data at 1000, 850, 700, 500, 400, 300, 250, 200, 150, and 100 mb) contains a maximum wind ("77" level in the TTAA in Table 1; "8" level in Table 2). This information is transmitted in addition to the PPBB levels because it is common for a maximum wind to occur between prescribed wind reporting levels. This information has been omitted from NCDC data. For the same 600 matched soundings discussed above, the greatest wind speed from the NCDC data often failed to duplicate the actual (GTS) maximum wind. Section 3.2 describes our efforts to acquire the original maximum wind from GTS data and insert it into the NCDC sounding.

2.3. Tropopause Data

The level of the tropopause has been flagged in the NCDC data since 1976; before 1976 this information was omitted. In addition, only the lowest tropopause (sometimes there is more than one) is included. The original computation of the tropopause height is performed using all available information from the rawinsonde, which may or may not get reported as mandatory or significant levels in the GTS transmission of the data. In other words, although a tropopause height can be recomputed from the reported levels supplied by NCDC for data before 1976, the real tropopause height cannot be recreated because unreported data could have been used in computing the original tropopause height. Section 3.3 describes a procedure for estimating a tropopause height to be inserted into the NCDC data when the original tropopause height from GTS data is not available (all data before 1980).

2.4. Mandatory-Level Heights Below the Surface

Information on mandatory-level height below the surface was included in the NCDC data before, but not after, 1970. Section 3.4 describes the procedure by which we calculated these heights hydrostatically. The 1000 and 850 mb heights appearing in Table 3 were added by our processing programs.

2.5. General Differences

Comparisons of GTS data with NCDC data reveal other differences. A sounding is considered hydrostatically consistent when the implied height difference (the thickness) between two adjacent mandatory pressure levels equals the difference of the (reported) heights of the same two levels (see Section 4 for a complete description of hydrostatic computations). For the most part, the NCDC temperature-height data are more consistent, hydrostatically. This is especially true for observations taken before 1970, for which the information was calculated

and transmitted by hand rather than by computer. Because computers replaced manual methods after 1980, most of the GTS data are also hydrostatically consistent. In either case, GTS thermodynamic data were not used for the FSL archive unless information was missing from the NCDC archive.

Differences in GTS and NCDC dewpoint depressions are worth noting. A comparison of the dewpoint temperatures in Tables 2 and 3 reveals a U.S. reporting practice in effect since 1973. All relative humidities less than 20% are reported operationally as 30°C dewpoint depressions and are archived at NCDC as 19%. Therefore, if relative humidity is computed from GTS data, it is possible that some of the 30°C dewpoint depressions convert to relative humidities less than 19%. Since all NCDC humidities less than 20% are set to 19%, when they are converted back to dewpoint depression, the dewpoint depression does not match what is contained in the GTS report. Therefore, when processing GTS data, the computer program should set the relative humidity to 19% whenever the dewpoint depression is reported as 30°C, and when processing NCDC data, should set the dewpoint depression to 30°C whenever the relative humidity is 19%. According to Wade (1991), the relative humidity sensor now used on U.S. radiosonde flights is accurate below 19%, and relative humidities of less than 19% could be reported. This reporting practice may change in the near future (Facundo, personal communication).

Neither NCDC nor decoded NSSFC data retain the information about the sounding that is usually transmitted in the GTS message at the end of the TTAA section. This information is referred to as regional or additional information, and it is preceded by the indicator group 51515. In North America, stations report a lifted index (which can be recomputed by the user) and a mean wind, usually for the surface to 5,000 ft and 5,000-10,000 ft MSL. Should the radiosonde instrument fail for any reason, additional coded information appears after the 51515 group to indicate the problem. Information in the TTBB section of the sounding preceded by the group 31313 pertains to the type of radiosonde in use and the actual time it was released; this too is not retained in the NCDC or NSSFC versions. When available, sonde type and reported release time are included in the FSL data base.

3. THE FSL DATA BASE

3.1. General Description

The FSL data base consists of rawinsonde data from 1946 to the present that are available from the sources described in Section 1. Because our research concerns the troposphere and lower stratosphere, data above 100 mb are not included in this archive. As mentioned, we obtained the NCDC data from NCAR because they were available to us at a much lower cost. There are minor problems

with NCAR data that should be noted. NCAR, in an effort to keep their archive as up-to-date as possible, acquires data from NCDC in near real time. But NCAR data before 1984 are not the most recent version of NCDC TD-6201 series data, and thus, NCAR data, and subsequently data in our data base from 1976 to 1984, do not contain the tropopause level or the flag that indicates generated significant levels. If we had acquired data directly from NCDC, we could have included these flags where they appeared in the data. In addition, since NCAR in effect acts as another processor of NCDC data before they enter our data base, any errors NCAR may have created (we have yet to find any) become part of our data set. Canadian data also were obtained from NCAR, which receives these data processed by AES.

As mentioned in Section 2, NSSFC was our source of GTS data for 1981 to 1986. Since 1986, FSL has received GTS data directly, and they are checked for quality as described in Section 4. NSSFC runs a decoder through the GTS reports to supply their operational forecasters with an early look at standard-level charts and to process data for local studies. The decoder has problems processing certain real-time data. As a result, the NSSFC data base contains occasional erroneous and incomplete soundings, and Canadian and Mexican data are particularly scarce. Unfortunately, NSSFC data for the 1970s have not been retrieved because they reside on old 7-track tapes, which we cannot read. NSSFC data have not been checked for quality since 1980 because Inman's (1968) original hydrostatic quality control program was not converted to run on their new computer system.

3.2. Merging Originally Transmitted Wind Information

Much of the data after 1980 in the FSL data base contain winds at thermodynamically significant levels (as provided by the NCDC) and at original GTS wind levels, as long as the reported sounding was available in both the NCDC and GTS archives. Wind information at the "6" levels are the originally transmitted GTS winds. Therefore, if winds are given in both the "5" (NCDC significant levels) and "6" levels, duplication, not additional detail, of the wind results.

The process of merging GTS wind data into NCDC data was tricky and deserves some discussion. The most important step in merging two soundings is to verify that they are from the same location and for the same time. The first check is to match the WBAN (Weather Bureau, Army, and Navy) station numbers assigned by NCDC to corresponding WMO numbers, which are the only numbers included with GTS data, by cross-referencing a station historical file. If the station numbers and times match, a final check is done by comparing the data. If the surface-level pressure and temperature are within 1°C and 1 mb, the soundings are considered to be the same. If the data are not already in the NCDC data set, then they are merged into the FSL data base as a new sounding. First, the raw data are input and the wind levels are extracted. Since the pressures for the

wind levels must be computed, they are set to missing so they can be recomputed in context of the NCDC sounding data. (The user of the data base can tell if GTS winds were merged into their data by examining the data source parameter, which is set to "2" if merged wind data exist [see Appendix A].)

If a maximum wind level ("77" level in the WMO coded message) is found in the GTS data, it too is merged into the NCDC sounding. The pressure at this level appears in the maximum wind index of the third identification line (see Appendix A) and also in the sounding as the "8" line. However, in cases where the original maximum wind is missing, and for data before 1980 for which we had no other data to merge, the user of the FSL data base will notice an entry for the pressure of the maximum wind in the identification line, but will not see an "8" entry in the data. We objectively searched all the wind data in the sounding and placed the pressure where the greatest wind is found in the identification line. This step gives some information for maximum wind in the identification line for users who may need it "up front" rather than having to search for it in the body of the sounding. When there is an entry for maximum wind and no corresponding "8" line, the pressure of the maximum wind is an estimate and not from the original GTS report.

3.3. Reclaiming and Estimating Tropopause Pressure

As with the maximum wind, NCDC does not retain tropopause data, the "88" level in GTS reports. We merged this information into NCDC thermodynamic data when it is available. However, for data before 1980, and for soundings after 1980 for which we could not find the GTS data, we estimated the pressure of the tropopause and inserted it into the identification line. When a "7" level appears in the data, the tropopause is from the GTS data; otherwise the tropopause pressure found in the identification line has been derived.

We use the WMO definition of the tropopause found in the Federal Meteorological Handbook No. 3 (U.S. Departments of Commerce and Defense, 1981) to compute the tropopause. Since the FSL data base does not include levels above 100 mb, a complete test for the existence of the tropopause may not always be possible. If data in a sounding meet the tropopause criteria, but testing stops because the 100 mb level has been reached, the tropopause index on the identification line will list the derived tropopause as suspect. For more information on the computer code that was used to estimate a tropopause, see Appendix C.

3.4. Adding Heights of Mandatory Pressure Levels Below the Surface

The FSL data base contains heights for all mandatory pressure levels regardless of their elevations, which may fall below the surface elevation of the station. Since 1970, the NCDC has omitted these below-surface heights, which were part of the originally transmitted GTS data. Since it is useful to have

these data for completeness, we recomputed missing mandatory-level heights and inserted them into our data base.

The hydrostatic relationship, discussed in detail in Section 4.1, can be used to estimate the height of a mandatory pressure surface when the temperatures at both adjacent levels are known. However, a problem arises when we apply this relationship to estimate the height of a pressure surface when the station pressure is less than the mandatory pressure, because the temperature at the mandatory surface does not exist. Therefore, we cannot apply the hydrostatic relationship directly because its use requires estimation of a fictitious mean virtual temperature. Saucier (1955) explains in considerable detail how the NWS computed the mean virtual temperature for these fictitious layers before 1970 (before computerization). This required averaging a current surface temperature, and a temperature from 6 hours earlier, as part of an estimate for the plateau correction for stations in the Rocky Mountains. Since 1970, the NWS has used the following algorithm to compute the virtual temperature (see Section 4.1 for the definition of the virtual temperature) for the mandatory-level surface that falls below the elevation of the station:

$$T_f = T_{av} + [FF(P_f + T_{av} - P_s - 223.15)], \quad (3.1)$$

where T_f equals temperature of the mandatory level below the surface (at a pressure, P_f , of 1000 or 850 mb), T_{av} equals the average of the current temperature (K) and the temperature at time $t - 12$, and P_s equals the surface pressure. The empirically derived constant FF varies according to the variation in average temperature, as shown in Table 4.

We did not apply either of these methods because we did not have the necessary surface temperature observations, and we did not learn of the NWS algorithm until most of our data had already been processed. The user can recompute the heights of mandatory levels below the surface using Eq. 3.1. To do so, the previous sounding or a surface observation at the site is needed for the temperature at $t - 12$. Then simply reapply the hydrostatic equation to calculate the required mandatory pressure surface. In this manner, the user will obtain a mandatory height that is similar to that from above.

Our method of estimating a fictitious temperature below the ground assumes that the current surface virtual temperature, and not some averaged value based on the temperature 6 or 12 hours ago, is sufficient to extrapolate downward below the surface. By doing so, we are ignoring part of the plateau correction included in the formulas previously described. To estimate the fictitious temperature below the ground, we first need to estimate how far under the ground this surface is by estimating the thickness (dz) of the fictitious layer defined by the surface elevation where the station pressure is measured and the mandatory-level

surface below the elevation of the station. The dz value can be computed by applying the hydrostatic equation (Eq. 4.4), assuming that the virtual temperature remains constant extrapolating downward. Thus, we use T_s , the virtual temperature of the surface, to approximate the average virtual temperature in the fictitious layer in the expression for dz :

$$dz = (RT_s/G)dp/P_s, \quad (3.2)$$

where P_s is the pressure at the surface, $dp = -(p_{\text{man}} - P_s)$, where p_{man} is either 1000 or 850 mb, R is the gas constant for dry air, and G is the gravity constant. From this estimate of dz we compute a temperature for the mandatory-level surface below the ground using the U.S. Standard Atmosphere lapse rate of $6.5^\circ\text{C km}^{-1}$.

The next step is to test the accuracy of the dz estimate with Eq. (4.4), using the average of the estimated virtual temperature of the mandatory-level surface and the surface virtual temperature as the mean virtual temperature for the layer, T_{avg} .

In practice, we solve Eq. (4.4) for the pressure of the mandatory-level surface and examine the error based on the dz estimate. With this pressure estimate error (p_{error}), we substitute back (p_{error} is used as dp) into the expression for dz above, and compute how much dz_{error} results because of p_{error} . We subtract this dz_{error} from the previous estimate of the thickness in the layer (to arrive at a new thickness estimate) and recompute a new temperature for the mandatory-level surface below the ground. Once again, the new thickness estimate is used to solve for the pressure at the bottom of the layer in Eq. (4.4). This process is iterated until the thickness of the layer between the surface and the mandatory level below the surface converges. Convergence is archived when the computed pressure at the bottom is equal to the pressure of the mandatory-level surface below the ground (in practice the estimate is considered equal if it is within 0.1 mb). Once the final thickness has been computed, the elevation of the mandatory level below the ground is simply the difference between the surface elevation and the computed thickness. The computer code that performs this iterative process is a subroutine in the hydrostatic check routine (see Appendix C).

4. OBJECTIVE HYDROSTATIC CHECKING AND CORRECTING

All data in the FSL data base are subjected to a hydrostatic error handling procedure that is designed to detect gross inconsistencies between observed temperatures and reported heights. A hydrostatic check cannot detect more serious errors sometimes found in rawinsonde data; for example, if a pressure cell fails, erroneous data may still exhibit hydrostatic consistency. The hydrostatic

check is most effective in detecting errors caused by encoding, faulty transmission signals, or incorrect computations. This section outlines the simple theory behind the procedure used in the application programs, much of which is a review of material discussed by Inman (1968).

4.1. Review of Basic Principles and Methodology

One of the best approximations in theoretical meteorology is the hydrostatic equation (Hess, 1959), which states that the vertical pressure gradient force exactly balances the force of gravity; i.e., $dp/dt = -\rho g$, where ρ is density and g is acceleration due to gravity. This equation can be integrated between any two isobaric surfaces, P_1 and P_2 , where $P_2 > P_1$ when virtual temperature is substituted for density using the equation of state. The virtual temperature is the temperature of a parcel of dry air having the same total pressure and density as that of the moist air parcel, i.e., an increase in temperature due to the lowering of air density due to water vapor at constant pressure. The following relationship is obtained:

$$H(P_1) - H(P_2) = (R_d/G)T_{av}^* \ln(P_2/P_1), \quad (4.1)$$

where H is the geopotential measured in meters, $R_d = 2.8704 \times 10^6 \text{ erg g}^{-1} \text{ K}^{-1}$ (gas constant for dry air), $G = 980.616 \text{ cm s}^{-2}$, the acceleration due to gravity, and T_{av}^* is the mean virtual temperature (K) in the layer.

If the mean virtual temperature in the layer defined by P_1 and P_2 can be calculated, the thickness of the layer can be found. In practice, the virtual temperature is computed using

$$T_{av}^* = T_{av} / (1 - 0.622Q_{av}), \quad (4.2)$$

where Q_{av} is the mean specific humidity in the layer. See Byers (1974) for the derivation.

Above 700 mb, $T_{av}^* - T_{av} < 1 \text{ K}$. Below 700 mb, the effect of moisture is such that T^* may differ from T by as much as 5 K (Saucier, 1955). Since our objective is to detect only gross errors, virtual temperatures are used in the hydrostatic checks below 700 mb and regular temperatures are used above that level. If the air temperatures were distributed according to the U.S. Standard Atmosphere in the 500-700 mb layer under saturated conditions, our practice of employing regular temperature and not virtual temperature could produce a 4-m error in the thickness of that layer and, subsequently, a 4-m error in the height of the 500-mb surface.

The mean temperature of a layer can be estimated by

$$T_{av} = (T_1 + T_2)/2. \quad (4.3)$$

When the actual temperature distribution in the layer deviates significantly from linearity, this estimation can introduce large errors into (4.1). This often is the case for deep layers, or layers in which there is a strong temperature inversion. When significant-level data are available in a layer bounded by mandatory levels, a logarithmic weighting scheme (see Section 4.4.2) using the additional temperatures at significant levels provides a better estimate of the mean temperature. However, in most applications, use of Eq. (4.3) is sufficient for gross error detection.

The thickness of any layer can be checked for consistency by evaluating the difference between the value obtained from the reported heights at the levels in question and the value computed from Eq. (4.1). We call the difference the delta (Δ) for that layer:

$$\Delta = H_1 - H_2 - \{[(R_d/G)T_{av}^*] \log_e(P_2/P_1)\}. \quad (4.4)$$

When Δ is large (see Section 4.2), errors can exist in the reported level temperatures, heights, or both.

The Δ 's for layers bound by mandatory pressure levels can be computed most readily from the reported temperatures and heights when the terms in Eq. (4.4) are grouped into a coefficient, Co :

$$\Delta = H_2 - H_1 - [Co(T_1 + T_2 + 546.32)], \quad (4.5)$$

where $Co = R_d/G \times \ln(P_2/P_1)$. Thus, each layer defined by mandatory pressure levels has a coefficient proportional to the difference of the natural logarithm of the bounding mandatory pressure levels, as shown in Table 5.

4.2. Delta Calibration

When using Eq. (4.5) to determine inconsistencies between reported temperatures and calculated heights, acceptable differences (or the allowable discrepancy, ϵ) must be established. If ϵ is selected too small (i.e., only a few meters), many Δ values will be flagged incorrectly because the method is not exact. Conversely, a large ϵ allows significant errors to pass undetected.

Inman (1968), in his application of Eq. (4.5), employed a calibration of Δ determined by Robstov, who performed an analysis of vertical temperature profiles in the Soviet Union. Since obtaining the original reference to this work was not practical, we determined typical values of Δ empirically from rawinsonde data

observations in North America. It is important to remember that most of these data have been subjected to quality control procedures at NCDC; we anticipated that the Δ values would be small and that they would vary over time owing only to differences in quality control and processing procedures at the NCDC.

We surveyed 7 years of data between 1950 and 1980 (1950, 1955, 1960, 1965, 1970, 1975, and 1980). Four seasonably representative months (January, April, July, and September) were chosen. The distribution of Δ 's we found was fairly uniform and varied only slightly from year to year and season to season. In Table 6, we present some statistics from a subset of approximately 1000 soundings in July 1975. The distribution in this table is typical of the different seasons and years surveyed. As anticipated, most of the Δ 's are small. Note the rarity of discrepancies greater than 20 m. In general, the number of larger Δ 's increases with the height and depth of the layers. These results indicate that, although errors are relatively rare, they do exist in the NCDC-processed data.

Based on this survey, we tried three to four times the absolute standard deviation of Δ as the value for ϵ . However, extensive testing determined that this value produced many small corrections to data that, upon closer inspection, should not require adjustment. So, we adjusted the ϵ 's upward (values in parentheses in Table 7) to be closer to those developed by Robstov and used by Inman (1968).

4.3 Hydrostatic Checking Procedures

Heights are computed from reported temperatures by starting with observed surface data and proceeding mandatory level by mandatory level, always assuming the information for the bottom of each layer (the surface data for the initial check) is correct. If a surface data error exists, hydrostatic checking is impossible because accurate data are required as a baseline for hydrostatic computations. Therefore, it is essential that the elevation of rawinsonde release point is known and that the correct pressure (baroswitch) and temperature calibrations have been made. In practice, checking surface data is difficult because NCDC does not archive the surface conditions that are part of the sounding observation. Because of their importance, surface data problems are discussed further in Section 4.4.

Equation (4.5) is used to search each sounding for errors in height, temperature, or both, by computing the Δ 's for the 10 mandatory pressure layers. The first Δ is computed for the layer bounded by the surface and the first mandatory layer above the surface. The Δ for the layer bounded by the first and second mandatory pressure level above the surface is computed next. This process continues upward until the last Δ , bounded at the top by the 100 mb level, is computed. Errors are detected by searching for two (and only two) consecutive Δ 's that exceed ϵ for their respective layer. When two isolated (the Δ 's below

and above the two layers in question fall below the allowable ϵ) consecutive Δ 's exceed the ϵ for their respective layers, the mandatory level in common between the two layers is likely in error. For example, if the Δ 's for the 850-700 mb and 700-500 mb levels are both greater than their respective ϵ 's, and the Δ 's above and below these two layers are smaller than their respective ϵ 's, the 700 mb level data are probably erroneous. When more than two consecutive Δ 's exceed the ϵ , adjustments to data become difficult to apply with confidence (see Section 4.3.3). On occasion, only an isolated Δ will exceed its ϵ . This special case is discussed in Section 4.3.2. The method for distinguishing height and temperature errors is described next.

4.3.1. Correcting Heights and Temperatures for Two Consecutive Large Deltas

When two consecutive large Δ 's are isolated and are of equal magnitude but opposite sign, then the height of the mandatory level shared by the two layers contains a simple height error (complex height errors are described below). In practice, equal magnitude occurs when the difference in the consecutive Δ 's is less than or equal to 20 m. The correction that is applied to the original height is

$$C_h = 1/2 [\Delta_{(\text{upper})} - \Delta_{(\text{lower})}], \quad (4.6)$$

where upper and lower indicate the upper and lower layers used in the computation. This type of error is the most common one detected, and the easiest to correct with confidence.

When two consecutive large Δ 's have the same sign and magnitudes that are equal proportionals of their respective coefficients, then an error exists in the temperature of the mandatory level common to the two layers. In practice, some tolerance in the definition of proportionality is allowed. The Δ for each layer is divided by its appropriate coefficient (Table 5). If the absolute difference between these quotients is ≤ 1 m, the Δ 's are considered proportional to their coefficients. The correction applied to the reported temperature is

$$C_t = 1/2 [\Delta_{(\text{lower})}/C_{o(\text{lower})} + \Delta_{(\text{upper})}/C_{o(\text{upper})}]. \quad (4.7)$$

This simple procedure is most effective for detecting and correcting temperatures that carry the wrong sign. Whenever a temperature is adjusted, another check is performed to ensure that a superadiabatic lapse rate has not been created as a result of the change (see Section 4.4.1). When it has been determined that the temperature correction is realistic, the dewpoint temperature is adjusted using the same correction. If the correction is unrealistic because a superadiabatic

lapse rate has been created, no correction is made to the reported temperature and the hydrostatic check stops.

When two consecutive Δ 's are large but do not appear to be simple errors of the types described above, corrections must be applied to both the temperature and height. If the initial Δ 's have opposite signs (but do not meet the criteria for equality), we presume on our experience is that most of the error is probably due to a height error. We then correct the height first, using

$$C_{HT} = [C_o(\text{lower}) \Delta_{(\text{upper})} - C_o(\text{upper}) \Delta_{(\text{lower})}] / [C_o(\text{lower}) + C_o(\text{upper})], \quad (4.8)$$

and the Δ 's are recomputed using the corrected height. The new Δ 's should have the same sign and be equal proportionals of their coefficients. Equation (4.7) is then applied to correct the temperature. Our experience indicates that most of the correction is accomplished with the initial height adjustment, generally resulting in very little adjustment to the temperature.

If the signs of the initial Δ 's are the same, but the values are not proportional to their coefficients, then most of the error is probably due to a temperature error, which we first correct using

$$C_{th} = [\Delta_{(\text{lower})} + \Delta_{(\text{upper})}] / [C_o(\text{lower}) + C_o(\text{upper})]. \quad (4.9)$$

The Δ 's are then recomputed using the corrected temperature, which should yield new Δ 's that are nearly equal but opposite in sign. At this point, a small adjustment can be made to the height using Eq. (4.6).

Equations (4.8) and (4.9) can be applied to all situations because they produce results that are equivalent to those of Eqs. (4.5) and (4.6) when they are applied to simple errors not requiring simultaneous adjustment of both heights and temperatures. (When Eqs. [4.8] and [4.9] are applied to simple errors, the recomputed Δ 's are nearly zero, requiring no further corrections.) But our correction procedure generally does not apply to Eqs. (4.8) and (4.9) unless initial calculations of the Δ 's indicate that using Eqs. (4.5) and (4.6) is inappropriate. This practice eliminates the unnecessary small second adjustments that arise from using Eqs. (4.8) or (4.9).

4.3.2. Correcting an Isolated Error

When computing the Δ 's for the 10 layers, it is possible to find a single, isolated Δ that exceeds ϵ . In this case, the error is most likely because an observer incorrectly computed the relative geopotential thickness between two layers. For example, if the 1000 and 850 mb heights were computed correctly but an error was made computing the 700 mb height, only the 850-700 (not the 700-500)

mb Δ will exceed the ϵ . This incorrect 700 mb height will cause all heights above 700 mb to be in error as well. In our correction procedure, this is treated as a major revision to the original report and is applied only when it is completely safe to do so.

To assure that it is safe, a more stringent test than the one applied to two consecutive Δ 's is applied to the isolated large Δ . This test requires that the isolated Δ exceed the ϵ by 150%. If the Δ exceeds ϵ , but by less than 150%, the hydrostatic check stops at the layer in question and no further corrections are applied to the sounding. When the Δ exceeds the ϵ by 150%, the correction made to the top level of the layer and all heights above this level is

$$C_h = -\Delta \quad (\text{layer}) \quad (4.10)$$

In practice, it is desirable to find the cause of the isolated Δ that is inconsistent. Section 4.4 discusses diagnostic tests for superadiabatic lapse rates, superinversions, and inaccurate estimates of the mean temperature that often result in large isolated discrepancies in (4.5).

4.3.3. Uncorrectable Errors: Three or More Consecutive Large Deltas

Soundings containing numerous errors are very difficult to correct. When more than two consecutive Δ 's exceed the ϵ 's, it is not safe to apply corrections to the data. For example, if all the 850-700, 700-500, and 500-400 mb Δ 's exceed their respective ϵ 's, both the 700-mb data and the 500-mb data are questionable and it is impossible to determine which, if not both, need to be corrected.

As with the isolated large Δ , our objective checking procedure performs additional diagnostics (discussed in Section 4.4) to verify the existence of three consecutive large Δ 's. In addition, if any two of the three large Δ 's have the characteristics described in Section 4.3.1 that require simple temperature or height corrections, these corrections are attempted and Δ 's are recomputed. If the Δ 's are successfully reduced by the simple height or temperature correction, the original situation of three large Δ 's is thus reduced to the isolated Δ situation.

4.4. Enhancements

Our experiences with the hydrostatic check procedure discussed in Section 4.3 lead us to believe that we needed more sophisticated diagnostic tests on the data than those employed by Inman's original application of the theory. For the most part, these additional tests are performed to ensure that the surface layer Δ computation is correct. These tests also ensure that other Δ 's exceeding their respective ϵ 's arise solely from inconsistencies between reported temperatures and calculated heights, and are not due to superadiabatic lapse rates, inver-

sions, or an inaccurate determination of the average mean virtual temperature in a layer. Since it is difficult to safely correct a sounding with more than two consecutive large Δ 's with any degree of confidence, and difficult in the case of the isolated large Δ , these additional tests should be applied to these situations as well. The goal is to reduce the Δ for any of the three, resulting in only two consecutive large Δ 's, i.e., a more desirable situation, or to eliminate the isolated large Δ altogether.

4.4.1. Checking for Superadiabatic Lapse Rates

When the surface layer Δ exceeds the ϵ , the objective procedure first checks for a superadiabatic lapse rate (super). The minimum depth of a layer that is checked is 50 mb; a layer is flagged as a super if the temperature decrease with height exceeds $9.8^\circ\text{C km}^{-1}$. One of the more common errors that this check flags and corrects effectively is an incorrect sign in the temperature for the surface or first mandatory level (often 1000 mb) above the surface. If the surface temperature has the erroneous sign, a super or an inversion is often created. The first test concerns a large surface Δ resulting from a super created by erroneous surface data. In this case, the sign of the surface temperature is reversed (with the additional condition that the absolute value of the temperature from the surface to the first mandatory level above the surface be greater than 20°C ; this additional check is a safeguard to ensure that the sign of the temperature and not some other error is truly responsible for the creation of the superadiabatic lapse rate) and the Δ is recomputed. When the incorrect sign is at the mandatory level above the surface, the Δ above the surface Δ would reflect this error as well; i.e., the first two Δ 's can have the same sign and equal proportionals to their coefficients if no other error is present. When this is the case, the standard temperature correction, Eq. (4.7), is applied.

The check for a super is also performed before accepting any isolated large Δ (other than the surface layer) or a third consecutive large Δ . Testing is done below and above the layer in question for minimum layers of 50 mb. If a super is found below (above) the layer in question, we try to correct the temperature and height for the bottom (top) level of the isolated erroneous layer. Before accepting any correction, a recheck is performed to see if the super no longer exists and if the recomputed Δ falls below the ϵ . If the super still exists or the Δ still exceeds the ϵ , the corrections are not retained and the original data are returned to their positions in the data array.

4.4.2. Applying a Pressure-Weighted Log-Average Temperature Calculation

Our hydrostatic check procedure is not appropriate when the atmosphere's temperature distribution with height varies greatly from linearity. A pressure-weighted log-average technique employing any significant-level data available in the layer is used to determine the mean virtual temperature for the layer if an

isolated large Δ is encountered, is in the surface layer, or is the third in a series of large Δ 's. By doing so, the magnitude of a Δ is often reduced. This correction often reduces the number of consecutive large Δ 's to two, a situation that can be corrected objectively, or eliminates the isolated large Δ .

When the sign of the surface temperature creates an inversion, the procedure is not as simple as setting a limit on the temperature increase with height. Arctic soundings often contain very steep inversions; there is no theoretical constraint on how much temperature can increase with height as there is with a temperature decrease (the autoconvective lapse rate). The checking routine assumes a nonlinear temperature distribution with height and recomputes the mean temperature using a pressure-weighted average temperature by using significant-level data. This often reduces the magnitude of the surface Δ . The computer code that performs this pressure-weighted log-average computation can be obtained by contacting the authors (see Appendix C).

4.4.3. Correcting Significant Level and Wind Level Data

In the introduction, we mentioned that archivers of GTS data must compute heights at significant pressure levels and pressures at WMO-defined wind levels. Only the pressure of significant levels and the height of wind levels are reported in GTS data. Therefore, it is necessary to correct some of these values whenever a correction is made to any mandatory level. This is because these added heights and pressures are computed using the mandatory-level data. For example, if erroneous data are corrected at 500 mb, all significant level heights and pressures at the wind levels between 700 and 500 mb and between 500 and 300 mb must be recomputed.

5. APPLYING HYDROSTATIC CHECKING PROCEDURES

This section provides examples of the techniques discussed in Sections 4.3 and 4.4. In addition, two examples of soundings with errors where no correction could be safely applied are described. These are only a few of the many situations that can be encountered, especially when processing real-time data. The reader is reminded that corrections should be attempted only for errors due to inconsistencies between reported temperatures and calculated heights. Errors resulting from other sources, such as bad pressure cells or thermistors, are not detectable with this procedure.

5.1 Correcting a Sounding with a Simple Height or Temperature Error

Table 8 is a sounding from Chihuahua, Mexico, with a temperature error at 300 mb. The original transmission indicated a 300 mb temperature of -27.7°C . The Δ 's computed from the objective hydrostatic checking routine for the 500-300 mb and 300-250 mb layers are -42 and -28 m, respectively. The scheme determined

that these Δ 's are nearly equal proportions of their respective coefficients (4.21 and 2.67, respectively; the quotients for these layers are 9.97 and 10.41), and the scheme applied a 10°C correction to the original temperature. Based on climatological values for the temperature at 300 mb, it seems quite reasonable that -37°C, not -27°C, was the actual 300 mb temperature.

Table 9 is a sounding with a height error at 850 mb. Note that the Δ 's for the 1000-850 mb and 850-700 mb layers are the only available ones exceeding the ϵ 's. Their signs are different but their magnitudes are nearly equal (within 20 m), indicating a problem with the height for the level shared between the two layers. The procedure determined that the reported height of 1341 m was too low by 196 m. The sounding is shown before and after to illustrate the effect of the objective procedure when a correction is made to a geopotential height. A correction is necessary for any computed significant-level height and significant wind-level pressure that originally fall in the 1000-850 mb and 850-700 mb layers because these quantities are computed using the 850 mb level height. For example, the wind level at 609 m had its pressure recomputed as 951 mb; the original computation was 943 mb.

5.2. Correcting a Sounding with a Simultaneous Height and Temperature Error

Section 4.3.1 discussed the situation when two successive Δ 's exceed the ϵ 's, but do not have magnitudes that would identify the error as a simple single correction to the height or temperature. This occurs when the signs of the two large Δ 's are the same and their magnitudes are not equal proportions of their respective layer coefficients, or when their signs are different and their magnitudes are not equal (within 20 m).

Table 10 is a sounding, in which both the height and the temperature are in error at 400 mb. Note that the 500-400 mb and 400-300 mb layer Δ 's exceed the ϵ 's and have opposite signs, but are not equal in magnitude. The objective routine recognizes this as a compound error involving a primary correction to the height and a secondary adjustment to the temperature. As the error message displays, 48.6 m was subtracted from the 400 mb height and 4.2°C was added to the temperature. As with any correction to the height, minor adjustments are made to significant-level heights and wind-level pressures for data that fall in the surrounding layers shared by the 400-mb level.

5.3. Recalculating the Pressure-Weighted Log-Average Mean Layer Temperature

Table 11 and Fig. 2 show a sounding taken into a deep arctic inversion, illustrating problems this kind of sounding can cause for computing the surface layer Δ . This sounding contains a marginally high surface Δ of 30 m, i.e., the discrepancy between reported temperatures and heights for the 966-850 mb layer if the 966 mb and 850 mb temperatures of -19.9°C and -0.5°C (the endpoints) are used

to compute the mean virtual temperature (-10°C). Using all the available significant-level data at and between 966 and 850 mb (941, 900, and 882 mb) to compute a log-weighted average temperature yields a mean virtual temperature of -2.5°C . This results in a Δ of only 2 m, well within the allowable ϵ . The net effect is a sounding that passes the hydrostatic check to 100 mb. If this additional recomputation had not been performed, the program would have flagged the surface Δ as exceeding the ϵ and no further hydrostatic checking would have been possible because of the large surface Δ . The top of the hydrostatic check (flag in the identification line of the archived sounding) would have been set to the surface pressure of 966 mb.

Table 12 and Fig. 3 depict a sounding with an interesting nonlinear temperature distribution between 700 and 500 mb. This is also a good example of a sounding that only appears to have an isolated inconsistent layer (the Δ for the 700-500 mb layer is 28 m, and is surrounded by Δ 's of 3 and 0 m). The objective procedure first recomputes the mean virtual temperature in the layer and a new Δ , before concluding it is an isolated inconsistent layer. The log-weighted procedure recomputes the temperature to be -12.7°C , compared with the -15.1°C computed using only the temperatures at the endpoints. The difference in the mean virtual temperatures accounted for a decrease in the Δ from 28 to 4 m. As a result of this recomputation, the objective procedure was able to continue checking to 100 mb and did not apply a correction to data at 700 mb and above, which would have been the case if the recomputed mean virtual temperature had failed to better estimate the real discrepancy in the layer.

5.4. Correcting a Sounding With an Isolated Inconsistent Layer

Table 13 is a sounding with an isolated, inconsistent 700-500 mb layer. The Δ of 46 m exceeds by 50% the ϵ for this layer and could not be reduced by recomputing the mean virtual temperature for that layer. The objective procedure subtracted 46 m from the heights at 500 mb and above at the mandatory levels. If this sounding had significant levels available, adjustments would have been made to these heights as well. Note that no changes were made to the heights of the wind levels, and thus their pressures, since these heights were originally transmitted data and are not tied to the heights at the surrounding mandatory pressure surfaces.

5.5. Uncorrectable Errors

Table 14 and Fig. 4 show a sounding that contains a superadiabatic lapse rate between 1000 and 850 mb. The Δ for this layer is -27 m. The objective procedure finds that a superadiabatic lapse rates exists and cannot improve the

discrepancy in the layer with a better estimation of the mean virtual temperature. This sounding passes the hydrostatic check to 1000 mb, which alerts the user to potential problems with data above 1000 mb.

Table 15 contains mandatory-level data for a sounding in which three consecutive Δ 's exceed their respective ϵ 's. In accordance with the discussion from Section 4.3, no correction was made to this sounding and the hydrostatic check terminated at 400 mb. It is obvious to those who are familiar with typical values of standard level heights that the height at 300 mb is in error. However, even though the Δ 's of the 400-300 mb and 300-250 mb layers are of opposite sign and quite large, they are not equal in magnitude. In addition, because the large Δ for the 250-200 mb layer suggests that the 250 mb data may also be erroneous, we are unsure about the contribution to the large 300-250 mb layer Δ from 250 mb data. Therefore we cannot assume that the 300-250 mb layer Δ is large only because of erroneous data at 300 mb. As a result of the uncertainty, the program cannot objectively make a correction to the data.

6. GROSS ERROR CHECKS

Gross error checking of the FSL rawinsonde data base covers point data checks, data level checks, and general sounding checks. Most of these checks either remove bad data or set them to missing; however, corrections are attempted when there are sufficient data.

6.1. Point Data Checks

Out of range data are the most common point data problem encountered. Pressure, height, temperature, and dewpoint are all checked against the bounds listed in Table 16. If dewpoint values are greater than their corresponding temperatures, both values are set to missing. Dewpoint values are also set to missing if the corresponding temperatures fall below -40°C . This mainly affects Canadian data since their sites do not follow the U.S. convention of cutting off dewpoints when the temperature falls below -40°C . In addition, if the magnitudes of the temperature are out of bounds in the positive sense but not in the negative sense, the sign of the temperature is reversed and later checked hydrostatically.

Other corrections to point data are made on a limited scale and only to satisfy the requirement that all levels have valid heights and pressures. Corrections to missing heights and pressures are made when sufficient real data are available. The hydrostatic equation uses significant-level or mandatory-level data to compute missing heights. In addition, a logarithmic interpolation in pressure using real heights is used to compute missing pressures. Missing pressures are most common in both the significant-level data from NCDC and the wind-level data from NSSFC or FSL GTS reports.

6.2. Data Line Checks

The second type of gross error check is a data line check. Valid pressures and heights are required for all data levels. Those levels that cannot be computed by gross error correction routines are removed. When a duplicate level is detected, the level with greatest number of missing fields is removed. A duplicate level is defined as a level that has the same pressure and level type (surface, mandatory, significant, or wind) as another level within the same sounding.

6.3. General Sounding Checks

Three general sounding checks were also performed. All soundings are required to have mandatory-level data above 700 mb, with one exception: Real-time data whose wind levels are merged with an NCDC sounding are required to have only surface and wind levels. The second type of sounding check, for duplicate soundings, is done by looking at the station and hour fields of the matrix file (see Section 7) from the data-base access files (Fig. 5) for duplicates. Finally, soundings that have fewer than five data levels are removed.

7. DIRECT ACCESS DATA RETRIEVAL

The FSL data base was created on a VAX VMS computer. Removable disk pack technology provides the platform around which the data set was designed. Since the data base was too large to store economically on disks, most of the data were written to magnetic tapes. Using a specialized disk/tape controller (Hierarchical Storage Controller), we can transfer a set of data files (2-4 years) from tape to disk pack in about 3 minutes. That makes the data base quite accessible; however, for convenience, six of the most recent data file sets (1981-1990; older data rotated off as new data are available) are permanently stored on disk packs. As computer storage technology continues to improve and become more economical, we plan to archive the data base on higher density CD-ROMS.

A magnetic tape of FSL data contains 2-4 years of data, depending on the years selected. This limitation was bounded by the physical capacity of the storage media (256 MB per disk pack). With the exception of the first disk pack, which has two sets, or 8 years of data, all the disks have one set of data files. Because the volume of data increases with each year since 1948, we are currently able to store only 2 years of data on a disk pack.

Three files are associated with every physical rawinsonde data base file once it has been transferred from magnetic tape to disk (Fig. 5). The "acc" (access) file and the "mtx" (matrix) file provide random access into the "fil" (data base) file. The acc file contains information on which time periods can be

found within the mtz file. The acc file is an unformatted, sequential, fixed-length (4 bytes) record file. Data contained within are read into a fixed size array of dimensions by year (4), by month (12), and by day/hour (62). Each day is divided into two time units: 0000 and 1200 UTC. Any odd hour data (i.e., special observations) between 0000 and 1200 UTC are stored in the 0000 UTC location. Likewise, data from 1200 to 2300 UTC are stored in the 1200 UTC location. Therefore, users who request data for 1500 UTC, for example, can retrieve any data that were available from 1200 through 2300 UTC. In addition, it is possible to access data valid only at synoptic (0000 or 1200 UTC) hour.

The mtz file contains information on every station's physical location in the fil file for any given time period. The mtz file is an unformatted, direct access, fixed-length (12 bytes) record file. Direct access record numbers are obtained from the acc file, which contains the number of records that follow for the specific time period. Data from the mtz file are read into a VAX structure that has three values defined: the record number for the fil file (4 bytes), the WBAN station number (4 bytes), and the hour of the station (2 bytes).

The fil file is an unformatted, direct access, fixed-length (16 bytes) record file. Data from the fil file are read through direct access file numbers provided by the mtz file. There are several different records in the fil file.

As an illustration, a typical access would work with the three types of files as follows. A sounding for WBAN station number 3131 is desired for 0000 UTC 2 January 1982. The accessing routine first copies the contents of the acc file into a working array, to locate which records within the mtz file need to be accessed. A starting record number for the mtz file is then received by the software. The direct access mtz access file can now be read. The first line input from this file contains the number of stations that follow for the requested time period. Successive entries in the mtz column contain the WBAN station number, the hour of the sounding, and the direct access line number, indicating the location of the actual data values in the fil file. The direct access line number given by the mtz entry for station number 3131 (6024) represents the first line of that sounding. A value within that line in the fil file is the number of lines that follow for that sounding. Therefore, once the starting line number for the sounding is known, the rest of the sounding in the fil file is accessible for output.

The station historical file (see Section 9 and Appendix B) plays a vital role for data retrieval. It contains information such as station latitude, longitude, surface elevation, and time period. The only station identification information physically stored in the direct access files are the WBAN station number and the date; therefore, when a sounding is requested, the station historical file must be accessed to obtain specific station identification information. Although a sounding may be in the data base, unless there is information

in the station historical file on that station for the date that the data is requested, it will not be possible to access it.

We have a separate station historical file for accessing the data base for two reasons. First, by not storing specific station historical information with every sounding, we are able to save 12 bytes of data for station location information for each sounding, which is a significant saving. Second, since we know that station history continues to change as we receive new data, we want to be able to update the sounding dynamically with the latest station identification information. Therefore, whenever a sounding is accessed, the historical information received will always be the latest. Although the station historical file may have the most accurate sounding location information, it may not match data in the sounding report. We have noticed discrepancies between the station history elevation and the height of the surface level in the sounding. Rather than change the surface height so it agrees with the height from the station history, we let the user determine which value is correct. As our information on station histories continues to improve, this problem will decrease.

8. DATA INVENTORIES AND PROCESSING STATISTICS

8.1. Inventories

There are three types of data inventory for the FSL data base: hourly, period of record, and full data. The hourly inventory file contains the total number of soundings for each reporting time in the data base. Table 17 shows a segment of the period-of-record inventory file, which gives the first and last date that a sounding can be found for all stations in the data base. We have also added the total number of soundings for each station's period of record along with the number of possible soundings, which is the number of days for the period of record multiplied by two, the number of regular observation times per day. (A complete listing of this file is available in Appendix B (2).)

The full-data inventory gives detailed information for every station for any 24-h period. Table 18 illustrates the format of the full inventory of WBAN station number 3131. In this example, San Diego reported at least once a day from 6 June 1956 through 5 April 1980, and there were 17,368 soundings for the period. (You may contact the authors for this type of detailed information about other stations.)

8.2. Processing Statistics

A number of statistics on the FSL data base are kept. Table 19 shows these statistics, valid for the most recent processing of the data. The statistics shown from 1946-1988 are for NCDC data only. The 1989 and 1990 statistics are for real-time GTS data. A time period is defined as a 12-h period starting

at 0000 or 1200 UTC.

During the 1950s, approximately 20 stations took observations four times daily. This explains the rise in average number of soundings per time period up until 1957, and then the sudden drop in 1958 when stations changed to two observations per day. In later years, special observations were taken, some of which may have been taken for field experiments. An example of this can be seen in 1979 and 1986, where the "max-snd" field rises well beyond the average. The significant drop in the average number of soundings reported for 1988 can be attributed to the lack of archived Canadian data. The FSL archive, as of this writing, has NCAR-supplied Canadian data up through 1987. The numbers rise again in 1989 and 1990 because Canadian data are available from FSL's GTS data source. More disturbing, though, is the general decline in the average number of soundings since 1977, which probably reflects the general decline in the number of stations taking observations in North America.

The statistics in Table 20 relate to the overall quality of the data set. Percentages were computed for the number of soundings having data up to various mandatory pressure levels, and on how many of these pass the hydrostatic check. For example, in 1960, 99.94% of the soundings went up to at least 700 mb. Overall, the completeness (how high in the atmosphere the sounding has data) of the data looks good. More than 93% of the soundings after 1955 have data up through the 300 mb level, and of these, 93% are hydrostatically consistent to 300 mb. Maximum quality values are highlighted for each parameter. There is little change in the statistics since 1960. Soundings that are not hydrostatically consistent up to 700 mb probably failed the hydrostatic check for the surface layer, probably because the surface height discrepancy discussed in Section 7. It is interesting to note that in recent years there has been a small decline in the number of soundings that are hydrostatically consistent up through 100 mb. The decline in this number since 1985 seems to coincide with the implementation of a fully automated observing system in the United States. We have noted an increase in the number of missing, erroneous, and incomplete soundings for the U.S. network. See Schwartz (1990) and Schwartz and Doswell (1991) for details concerning data quality within the last few years.

9. STATION HISTORICAL DOCUMENTATION

To our knowledge, a comprehensive, complete, and accurate station history for North American upper-air stations does not exist. We have undertaken considerable effort to compile and document as much historical information as possible. This is an ongoing activity, as we continue to learn more about where stations are, where they have been, where they are moving to, how they are identified (WBAN and WMO numbers), and, most important for research, their elevation.

NCDC and others launched similar efforts in the past. Most notable was

that of the Weather Bureau in 1964. The document entitled "Key to Meteorological Records and Documentation No. 5.21, History and Catalogue of Upper Air Data for the Period 1946-1960" (U.S. Department of Commerce, 1962) is an excellent early reference for information on U.S.-controlled stations. In addition to providing basic station location, identification, and elevation information, this publication reviews the type of equipment in use from the beginning of the upper-air program in 1937 through the early 1960s. Contact the NCDC for a copy of this document since it is no longer available through the U.S. Government Printing Office and may not be available through your library. This is our and NCDC's primary source of historical information up through 1960.

In 1973, NCDC issued an in-house (unpublished) paper entitled "Historical Documentation of Upper Air Observations of All U.S. Services." We were unable to ascertain how the information in this document was acquired; however, our experience using and checking the information suggests that it is some of the only reliable historical information available through 1973. In addition, it is the only source of information on Canadian upper-air sites that we have found. In 1977, NCDC produced another unpublished, abbreviated upper-air history. This compilation of information relied on handwritten memos, telephone conversations, and official correspondences between NCDC and the reporting sites themselves. Our experience with this publication has not been as favorable as with what was done in 1973.

We were able to obtain only some of the original Weather Bureau A1 forms from the various regions within the NWS. These A1 forms are the official documentation describing station moves, equipment changes, etc., associated with all NWS operational offices. We requested these forms in an attempt to verify the documentation we received from NCDC. The response to our inquiries varied. For example, documentation sent to us from the Western Region was extensive whereas very little was available from the Eastern Region. In addition, a student from the University of Virginia had hand-compiled the previously mentioned telephone memos and correspondence NCDC had saved on summary sheets for each upper air station. It remains a mystery to us what has happened to the documentation the student used and to many of the original A1 forms.

The AES has been contacted concerning the Canadian stations. Although most of the Canadian histories seem to be known in NCDC, there is a problem in identifying the elevations at many of these sites. For example, in the NCAR archive, many of the elevations of the Canadian stations were erroneously identified. In many instances, the elevations of nearby hourly observing sites are used instead of the elevation at the raob observing site. In some instances, these elevations can differ by as much as 100 m. We are working with the AES and NCAR to correct these problems.

The station historical information in Appendix B (2) was compiled by cross-checking all the above-mentioned references. In many instances, we were forced to act as referee when discrepancies arose. In cases where there were more than two sources of information, the majority ruled. Some entries have question marks or comments because we were unable to locate the necessary information to make a valid entry. We hope to eliminate these gaps as we learn more about these histories. Entries have been made for every station we know about that ever took rawinsondes and that are currently taking them. We exclude stations that were open for less than one month and stations that were open only for special observational experiments. Since the station history is a continuing effort, the results we present here are still preliminary. This history can be obtained in digital form by contacting the authors.

9.1. Basic Station Historical Information

The first station historical file contains basic history, i.e., station name, WMO and WBAN identifiers, latitude and longitude, and cross-reference information. Table 21 describes the entries in the digital file (see Appendix B (2)). Most stations have multiple entries. A new entry is made for a station when any parameter in the entry is no longer valid, e.g., if a station changed latitude or longitude, station elevation, etc. The dates that appear are the valid times for the current entry, and a 99 for year, month, or day indicates that this information is unknown. A blank ending date indicates that the station is open as of this writing.

Each entry normally is followed by a blank column, but a question mark immediately following an entry indicates that the entry is questionable and should be used with caution. Blanks for three-letter identifiers indicate that we could not determine if the station had one. All stations have WBAN numbers, but not all have WMO numbers. Note that the WBAN number is unique, but the WMO number is not. For example, WMO number 72293 was used for San Clemente Island, California, and is currently used for San Diego (Miramar Naval Air Station), California, but each has its own WBAN number.

To make this history more useful, we tried to track stations that changed location and WBAN number. The number in columns 88-92 is the WBAN number that this station had previously been identified by. The number in columns 94-98 is the WBAN number the station moved to. In this manner, one can follow the relocation of principal observational sites through the years. For a few stations, the entry for the "from" and "to" location is the same. This is not an error. For example, the Oklahoma City, Oklahoma, area station started as WBAN number 13967, moved to 13919, then to 3948, back to 13967, and then back to 3948 again. The WBAN number in columns 100-104 indicates that there is another station that should be referenced when accessing data for this station. In most

cases, the cross-referenced station records winds only. If a "W" appears in column 106, this indicates that this station took wind observations only and data for the station may not be in the archive. The comments beginning in column 108 further explain some of the questionable entries and may contain other useful information about the station.

9.2. Equipment Historical Information

The second file contains information we compiled about types of equipment used at the various sites and is listed in Appendix B (3). This information is incomplete for many sites, especially secondary sites, that were not in operation for a long time, and Canadian and Mexican sites. The records that appear in this file are 80 columns long, but are of variable number. For any given station, depending on how many changes to instrumentation were made and what information we were able to acquire for the station, a variable number of lines appear. Table 22 is a description of the entries in this file.

10. CONCLUDING REMARKS

In this memorandum we describe the creation of a complete, research-quality, upper-air data base for North America from 1946 to the present. The most important reason for creating and updating this data base was to support research within FSL and affiliated research organizations. The FSL data base, because of its direct-access format, is well suited to support research requiring long-term access to upper-air data, such as climatological and statistical studies. Because an effort has been made to acquire data not found in NCDC's data base for North America, the FSL data base is also excellent for the researcher interested in individual meteorological case studies requiring a complete set of observations.

Much of the knowledge of upper-air data that has been conveyed here was acquired through working with NCDC data and real-time data for the FSL data base. Because the FSL data base is updated daily with GTS data and eventually with NCDC data, we will continue to become more knowledgeable about these data. As mentioned in Section 9, the station history remains an open-ended project. Interest in the station history for upper air has risen in recent years because climatologists need radiosonde data to investigate scientific issues concerning global warming and climate change. Updated information will be added to the station history as we receive it.

We are also continuing our efforts to acquire data previously thought to be lost and military data that have not been digitized. We consider the acquisition of any historical radiosonde data for the FSL data base a top priority. We are also continuing to cooperate with the NCDC and NCAR so that improvements and corrections to upper-air data can benefit a wide range of users of these data

bases. The authors encourage users of the FSL data base to keep us informed about problems and errors in the data so that we can continue to improve the quality of our data for future researchers.

II. REFERENCES

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TABLE 1

GTS RAWINSONDE REPORT
FROM 0000 UTC, 1 AUGUST 1986, FOR DENVER, COLORADO

72469	TTAA	51001	72469	99841	27867	32008	00080	////	////
85519	////	////	70191	12056	12514	50591	07960	26032	40761
20561	28047	30967	35980	26548	25091	451//	27051	20237	555//
27055	15417	621//	26550	10664	671//	24015	88129	657//	27540
77184	27567	41521	51515	10164	00052	10194	////	05009=	
72469	TTBB	5100/	72469	00841	27867	11833	25466	22700	12056
33647	08464	44621	05659	55537	03761	66513	06557	77481	10365
88459	12362	99444	13580	11367	26159	22353	28164	33278	39780
44222	519//	55129	657//	66113	637//	77100	671//=		
PPBB	51000	72469	90067	32008	33508	01007	9089/	08007	11010
91124	12012	13508	28514	9168/	29522	26030	92013	26034	26535
29043	925//	28047	9305/	26548	26549	9425/	27565	26058	9504/
27540	23515=								

TTAA: Mandatory level data

TTBB: Significant level data

PPBB: Regional and significant wind levels

TABLE 2

NSSFC DECODED GTS RAWINSONDE REPORT
FROM 0000 UTC, 1 AUGUST 1986, FOR DENVER, COLORADO

LEV	PRES	HGHT	TEMP	DEWPT	DIR	SPD
4	1000	80	32767	32767	32767	32767
4	850	1519	32767	32767	32767	32767
9	841	1611	278	108	320	8
5	833	1695	254	94	32767	32767
6	820	1828	32767	32767	335	8
6	792	2133	32767	32767	10	7
6	764	2438	32767	32767	80	7
6	737	2743	32767	32767	110	10
4	700	3191	120	60	125	14
6	687	3352	32767	32767	120	12
6	662	3657	32767	32767	135	8
5	647	3845	84	-56	32767	32767
5	621	4182	56	-34	32767	32767
6	614	4267	32767	32767	285	14
6	570	4876	32767	32767	295	22
5	537	5350	-37	-147	32767	32767
6	528	5486	32767	32767	260	30
5	513	5710	-65	-135	32767	32767
4	500	5910	-79	-179	260	32
6	488	6096	32767	32767	260	34
5	481	6211	-103	-253	32767	32767
6	469	6400	32767	32767	265	35
5	459	6571	-123	-243	32767	32767
5	444	6825	-135	-435	32767	32767
6	433	7010	32767	32767	290	43
4	400	7610	-205	-315	280	47
6	399	7620	32767	32767	280	47
5	367	8240	-261	-351	32767	32767
5	353	8520	-281	-421	32767	32767
6	323	9144	32767	32767	265	48
4	300	9670	-359	-659	265	48
5	278	10194	-397	-697	32767	32767
6	259	10668	32767	32767	265	49
4	250	10910	-451	32767	270	51
5	222	11696	-519	32767	32767	32767
4	200	12370	-555	32767	270	55
6	187	12801	32767	32767	275	65
8	184	12945	32767	32767	275	67
6	161	13716	32767	32767	260	58
4	150	14170	-621	32767	265	50
7	129	15091	-657	32767	275	40
6	126	15240	32767	32767	275	40
5	113	15898	-637	32767	32767	32767
6	103	16459	32767	32767	235	15
4	100	16640	-671	32767	240	15

LEV: level type (4=mandatory, 5=significant, 6=wind, 7=tropopause, 8=max wind, 9=surface; 32767 denotes missing or unreported value)

PRES: Pressure (mb)
 HGHT: Height (m)
 TEMP: Temperature (tenths Celsius)
 DEWPT: Dewpoint temperature (tenths Celsius)
 DIR: Wind direction (degrees)
 SPD: Wind speed (knots)

TABLE 3

NCDC ARCHIVE RADIOSONDE DATA
FROM 0000 UTC, 1 AUGUST 1986, FOR DENVER, COLORADO

LEV	PRES	HGHT	TMPC	DEWPT	DIR	SPD
9	841	1611	278	109	320	8
4	1000	49	32767	32767	32767	32767
4	850	1516	32767	32767	32767	32767
5	833	1697	254	88	327	8
5	800	2051	223	88	357	6
5	750	2607	172	81	102	8
4	700	3192	121	57	123	14
5	650	3810	87	-45	154	4
5	647	3848	84	-54	178	2
5	621	4185	56	-37	285	12
5	600	4466	35	-79	294	18
5	595	4533	29	-90	295	18
5	554	5106	-22	-105	277	23
5	550	5164	-25	-112	275	23
5	537	5353	-36	-149	266	25
5	513	5713	-64	-129	260	29
4	500	5913	-78	-176	260	32
5	481	6213	-102	-248	263	35
5	459	6572	-122	-242	279	36
5	450	6723	-129	-283	285	39
5	444	6826	-134	-320	287	41
4	400	7609	-204	-315	278	47
5	367	8239	-261	-349	279	54
5	353	8519	-261	-427	278	52
5	350	8583	-285	-430	278	52
5	321	9195	-324	-477	264	47
4	300	9669	-358	-510	266	48
5	278	10194	-396	-543	264	47
4	250	10912	-451	32767	269	51
5	222	11694	-518	32767	275	49
4	200	12365	-554	32767	270	55
5	175	13208	-598	32767	276	60
5	174	13244	-600	32767	274	58
4	150	14166	-621	32767	264	50
5	142	14505	-617	32767	270	43
5	129	15094	-657	32767	274	39
5	125	15285	-658	32767	273	37
5	122	15433	-659	32767	270	35
5	113	15901	-636	32767	260	21
5	109	16121	-659	32767	254	17
4	100	16643	-670	32767	238	15

PRES: Pressure (mb)
 HGHT: Height (m)
 TEMP: Temperature (tenths Celsius)
 DEWPT: Dewpoint temperature (tenths Celsius)
 DIR: Wind direction (degrees)
 SPD: Wind speed (knots)

TABLE 4

EMPIRICAL CONSTANT USED BY THE NATIONAL WEATHER SERVICE
TO COMPUTE HEIGHT OF MANDATORY PRESSURE SURFACE
BELOW THE ELEVATION OF A STATION

FF	Condition
0.020	T < 273.15K avg
0.025	273.15K < T < 283.15K avg
0.030	T > 283.15K avg

Table 5

VALUE OF THE COEFFICIENT (C_0), PROPORTIONAL TO THE DIFFERENCE
OF THE LOG OF BOUNDING MANDATORY PRESSURE LEVELS,
USED IN EQUATION 4.5.

Bounding levels (mb)	C_0
1000-850	2.38
850-700	2.84
700-500	4.93
500-400	3.27
400-300	4.21
300-250	2.67
250-200	3.27
200-150	4.21
150-100	5.94

TABLE 6

DISTRIBUTION OF ALLOWABLE DISCREPANCIES (DELTAS) FOR LAYERS
 BOUNDED BY THE INDICATED MANDATORY LEVELS.
 APPROXIMATELY 1000 SOUNDINGS TAKEN FROM July 1975 WERE SURVEYED.
 (ALL DATA ARE IN METERS.)

	Layer (x 10 mb)								
	100/85	85/70	70/50	50/40	40/30	30/25	25/20	20/15	15/10
Sample size	999	1000	994	985	976	972	965	951	943
Mean alg. error	3.8	2.1	3.4	1.6	0.5	0.0	-1.3	-2.3	-10.3
Mean abs. error	5.4	3.8	6.0	2.3	2.3	1.0	2.1	5.6	12.5
Abs std. dev.	4.8	3.6	4.5	1.8	2.3	1.1	2.9	4.9	-9.3
Distribution									
<1	287	255	240	353	459	653	618	358	247
1-5	384	589	384	584	449	312	263	256	138
6-10	207	189	249	48	60	6	64	216	154
11-15	89	26	89	0	8	1	18	82	170
16-20	25	5	25	0	0	0	2	31	103
21-25	4	4	5	0	0	0	0	8	56
26-30	3	2	0	0	0	0	0	0	43
31-35	0	0	2	0	0	0	0	0	14
36-40	0	0	0	0	0	0	0	0	7
41-45	0	0	0	0	0	0	0	0	6
46-50	0	0	0	0	0	0	0	0	2
>50	0	0	0	0	0	0	0	0	1

TABLE 7

ABSOLUTE VALUE OF ALLOWABLE DISCREPANCIES (DELTAS) FOR EACH
 MANDATORY LAYER (FROM RUBSTOV AND ADAPTED BY INMAN, 1968).
 NUMBERS IN PARENTHESIS ARE VALUES USED BY THE FSL
 OPERATIONAL HYDROSTATIC CHECKING ROUTINE.

Layer (mb)	Delta (m)
1000-850	25 (21)
850-700	30 (20)
700-500	40 (25)
500-400	30 (20)
400-300	35 (20)
300-250	35 (20)
250-200	40 (25)
200-150	45 (30)
150-100	50 (35)

TABLE 8

DECODED GTS RAWINSONDE REPORT FROM 1200 UTC, 2 MAY 1990, FOR CHIHUAHUA, MEXICO (WMO STATION 76225), DEPICTING A SIMPLE TEMPERATURE ERROR AT 300 MB. ONLY THE DATA AND DELTAS (VALUE FOR EACH DELTA SHOWN AT TOP OF LAYER) SURROUNDING THE ERRONEOUS DATA ARE SHOWN. CORRECTIVE ACTION TAKEN BY THE HYDROSTATIC CORRECTION SCHEME SHOWN BELOW.

LEV	PRES	HGHT	TEMP	DEWPT	DIR	SPD	DELTA
4	400	7450	-221	-521	250	47	-2
6	390	7620	32767	32767	250	49	
5	368	8057	-265	-271	32767	32767	
6	359	8229	32767	32767	250	71	
5	358	8255	-277	-357	32767	32767	
5	336	8707	-315	-405	32767	32767	
5	332	8791	-323	-359	32767	32767	
5	322	9006	-335	-345	32767	32767	
6	315	9144	32767	32767	255	74	
4	300	9500	-277	-289	260	74	-42
6	252	10668	32767	32767	260	91	
4	250	10730	-475	32767	260	92	-28
6	220	11582	32767	32767	255	98	
8	219	11584	32767	32767	255	98	
4	200	12170	-595	32767	255	90	4

76225 1990 MAY 1 1200 UTC; ERROR AT 300 MB
 -10.2 DEG ADDED NEW TEMP= -378

PRES: Pressure (mb)
 HGHT: Height (m)
 TEMP: Temperature (tenths Celsius)
 DEWPT: Dewpoint temperature (tenths Celsius)
 DIR: Wind direction (degrees)
 SPD: Wind speed (knots)

TABLE 9

DECODED GTS RAWINSONDE REPORT FROM 1200 UTC, 2 JANUARY 1984, FOR QUILLAYUTE, WASHINGTON, SHOWN BEFORE AND AFTER (BOTTOM) HYDROSTATIC CORRECTION OF THE HEIGHT AT 850 MB. ONLY THE DATA AND DELTAS (THE VALUE OF EACH DELTA SHOWN AT THE TOP OF EACH LAYER) SURROUNDING THE ERRONEOUS DATA ARE SHOWN. NOTE THE CORRECTIONS TO THE HEIGHTS OF THE SIGNIFICANT LEVELS AND PRESSURES OF THE WIND LEVELS BETWEEN 1000 AND 850 MB AND 850 AND 700 MB.

LEV	PRES	HGHT	--- BEFORE ---		DIR	SPD	DELTA
			TEMP	DEWPT			
9	1017	56	88	82	170	12	
4	1000	196	76	69	170	21	
6	985	304	32767	32767	170	29	
6	943	609	32767	32767	180	36	
5	933	684	58	47	32767	32767	
6	903	914	32767	32767	215	37	
5	873	1152	72	60	32767	32767	
6	865	1219	32767	32767	245	40	
5	859	1266	88	75	32767	32767	
4	850	1341	80	67	245	45	-198
6	806	1828	32767	32767	245	51	
6	779	2133	32767	32767	245	53	
6	754	2438	32767	32767	245	61	
6	729	2743	32767	32767	245	59	
4	700	3115	-7	-41	245	60	194
6	653	3657	32767	32767	245	62	
6	604	4267	32767	32767	245	58	
6	558	4876	32767	32767	245	73	
6	537	5181	32767	32767	250	82	
4	500	5730	-157	-217	245	70	4

LEV	PRES	HGHT	--- AFTER ---		DIR	SPD	DELTA
			TEMP	DEWPT			
9	1017	56	88	82	170	12	
4	1000	196	76	69	170	21	
6	987	304	32767	32767	170	29	
6	951	609	32767	32767	180	36	
5	933	765	58	47	32767	32767	
6	916	914	32767	32767	215	37	
6	883	1219	32767	32767	245	40	
5	873	1310	72	60	32767	32767	
5	859	1444	88	75	32767	32767	
4	850	1537	80	67	245	45	
6	820	1828	32767	32767	245	51	
6	790	2133	32767	32767	245	53	
6	761	2438	32767	32767	245	61	
6	733	2743	32767	32767	245	59	
4	700	3115	-7	-41	245	60	
6	653	3657	32767	32767	245	62	
6	604	4267	32767	32767	245	58	
6	558	4876	32767	32767	245	73	
6	537	5181	32767	32767	250	82	
4	500	5730	-157	-217	245	70	

PRES: Pressure (mb)
 HGHT: Height (m)
 TEMP: Temperature (tenths Celsius)
 DEWPT: Dewpoint temperature (tenths Celsius)
 DIR: Wind direction (degrees)
 SPD: Wind speed (knots)

TABLE 10

DECODED GTS RAWINSONDE REPORT FROM 0000 UTC, 21 JUNE 1990, FOR HUNTINGTON, WEST VIRGINIA, SHOWN BEFORE (TOP) AND AFTER (BOTTOM) HYDROSTATIC CORRECTION TO BOTH THE HEIGHT AND TEMPERATURE AT 400 MB. ONLY THE DATA AND DELTAS (SHOWN AT THE TOP OF EACH LAYER) SURROUNDING THE ERRONEOUS DATA ARE SHOWN.

--- BEFORE ---							
LEV	PRES	HGHT	TEMP	DEWPT	DIR	SPD	DELTA
4	500	5820	-69	-115	265	52	12
6	482	6096	32767	32767	270	56	
5	448	6669	-109	-179	32767	32767	
4	400	7530	-169	-269	270	52	62
6	395	7620	32767	32767	270	52	
6	363	8229	32767	32767	270	49	
5	348	8559	-245	-291	32767	32767	
6	320	9144	32767	32767	260	49	
4	300	9630	-325	-425	260	50	-31
5	278	10161	-371	-441	32767	32767	
5	276	10208	-561	32767	32767	32767	
6	256	10668	32767	32767	245	53	
4	250	10830	-623	32767	245	55	-6
--- AFTER ---							
LEV	PRES	HGHT	TEMP	DEWPT	DIR	SPD	
4	500	5820	-69	-115	265	52	
6	483	6096	32767	32767	270	56	
5	448	6673	-109	-179	32767	32767	
4	400	7531	-157	-227	270	52	
6	395	7620	32767	32767	270	52	
6	364	8229	32767	32767	270	49	
5	348	8566	-245	-291	32767	32767	
6	321	9144	32767	32767	260	49	
4	300	9630	-325	-425	260	50	
5	278	10161	-371	-441	32767	32767	
5	276	10208	-561	32767	32767	32767	
6	257	10668	32767	32767	245	53	
4	250	10830	-623	32767	245	55	

72425 1990 JUNE 21 00 UTC BOTH T AND H CORR AT 400MB
 4.2 DEG ADDED NEW T= -15.7 DEG -48.6M ADDED NEW HT= 7531 M

PRES: Pressure (mb)
 HGHT: Height (m)
 TEMP: Temperature (tenths Celsius)
 DEWPT: Dewpoint temperature (tenths Celsius)
 DIR: Wind direction (degrees)
 SPD: Wind speed (knots)

TABLE 11

DECODED GTS RAWINSONDE REPORT FROM 0000 UTC, 1 JANUARY 1984, FOR FORT NELSON, B.C., CANADA (SEE FIG. 2), ILLUSTRATING THE EFFECT OF A STRONG TEMPERATURE INVERSION ON THE CALCULATION OF THE SURFACE LAYER (966-850 MB) DELTA. ONLY DATA SURROUNDING THE SURFACE LAYER ARE SHOWN.

LEV	PRES	HGHT	TEMP	DEWPT	DIR	SPD
4	1000	124	32767	32767	32767	32767
9	966	379	-199	-225	0	0
5	941	579	-71	-77	32767	32767
5	900	933	24	-66	32767	32767
5	882	1097	22	-68	32767	32767
4	850	1395	-5	-95	270	26
5	750	2379	-99	-144	32767	32767
5	702	2886	-135	-195	32767	32767
4	700	2908	-137	-197	300	29

***** Surface Delta Computation *****

30 m Using simple mean virtual temp of -10.0

2 m Using log average mean virtual temp. of -2.5

PRES: Pressure (mb)
 HGHT: Height (m)
 TEMP: Temperature (tenths Celsius)
 DEWPT: Dewpoint temperature (tenths Celsius)
 DIR: Wind direction (degrees)
 SPD: Wind speed (knots)

TABLE 12

DECODED GTS RAWINSONDE REPORT FROM 1200 UTC, 1 JANUARY 1984, FOR WASHINGTON, D.C. (SEE FIG. 3), ILLUSTRATING THE EFFECT OF A NON-LINEAR TEMPERATURE DISTRIBUTION UPON THE CALCULATION OF THE 700-500 MB DELTA. ONLY DATA AND DELTAS (VALUE OF EACH DELTA SHOWN AT THE TOP OF EACH LAYER) SURROUNDING THE NON-LINEAR TEMPERATURE DISTRIBUTION ARE SHOWN.

LEV	PRES	HGHT	TEMP	DEWPT	DIR	SPD	DELTA
4	850	1569	-51	-151	330	15	3
5	834	1718	-59	-129	32767	32767	
5	825	1804	-57	-357	32767	32767	
6	822	1828	32767	32767	305	18	
5	814	1909	-41	-181	32767	32767	
5	794	2106	-47	-80	32767	32767	
6	791	2133	32767	32767	305	19	
6	761	2438	32767	32767	310	21	
6	732	2743	32767	32767	310	23	
5	717	2902	-101	-103	32767	32767	
5	707	3012	-79	-81	32767	32767	
4	700	3089	-83	-85	305	28	3
5	682	3291	-83	-92	32767	32767	
5	669	3442	-71	-131	32767	32767	
6	651	3657	32767	32767	305	28	
5	627	3945	-103	-153	32767	32767	
6	626	3962	32767	32767	305	22	
5	614	4107	-93	-243	32767	32767	
6	601	4267	32767	32767	310	18	
6	555	4876	32767	32767	325	22	
6	533	5181	32767	32767	325	21	
4	500	5660	-219	-379	315	23	28*
6	471	6096	32767	32767	310	27	
5	467	6158	-251	-551	32767	32767	
6	451	6400	32767	32767	305	29	
4	400	7260	-347	-497	310	33	0

*700-500 mb delta computed from simple mean temperature of -15.1 = 28 m
 computed from log average temperature of -12.7 = 4 m

PRES: Pressure (mb)
 HGHT: Height (m)
 TEMP: Temperature (tenths Celsius)
 DEWPT: Dewpoint temperature (tenths Celsius)
 DIR: Wind direction (degrees)
 SPD: Wind speed (knots)

TABLE 13

DECODED GTS RAWINSONDE REPORT FROM 0000 UTC, 4 MARCH 1981, FOR MONETT, MISSOURI, DEPICTING AN ISOLATED INCONSISTENT LAYER AT 500 MB. DATA AND DELTAS (VALUE OF EACH DELTA SHOWN AT THE TOP OF EACH LAYER) SURROUNDING 500 MB SHOWN BEFORE (TOP) AND AFTER (BOTTOM) SUCCESSIVE CORRECTION OF 46 M IS APPLIED TO MANDATORY LEVEL HEIGHTS AT AND ABOVE 500 MB.

LEV	PRES	--- BEFORE ---			DIR	SPD	DELTA
		HGHT	TEMP	DEWPT			
4	700	2998	-9	-9	205	24	3
6	669	3352	32767	32767	200	17	
6	644	3657	32767	32767	205	19	
6	596	4267	32767	32767	215	25	
6	552	4876	32767	32767	220	27	
6	531	5181	32767	32767	220	31	
4	500	5650	-165	-415	225	36	46
6	471	6096	32767	32767	235	45	
4	400	7300	-257	-279	245	71	3
6	399	7315	32767	32767	245	72	
6	382	7620	32767	32767	245	72	
6	308	9144	32767	32767	255	79	
4	300	9320	-419	32767	255	83	3

LEV	PRES	--- AFTER ---			DIR	SPD
		HGHT	TEMP	DEWPT		
4	700	2998	-9	-9	205	24
6	669	3352	32767	32767	200	17
6	644	3657	32767	32767	205	19
6	596	4267	32767	32767	215	25
6	552	4876	32767	32767	220	27
6	531	5181	32767	32767	220	31
4	500	5604	-165	-415	225	36
6	471	6096	32767	32767	235	45
4	400	7254	-257	-279	245	71
6	399	7315	32767	32767	245	72
6	382	7620	32767	32767	245	72
6	308	9144	32767	32767	255	79
4	300	9274	-419	32767	255	83

PRES: Pressure (mb)
 HGHT: Height (m)
 TEMP: Temperature (tenths Celsius)
 DEWPT: Dewpoint temperature (tenths Celsius)
 DIR: Wind direction (degrees)
 SPD: Wind speed (knots)

TABLE 14

DECODED GTS RAWINSONDE REPORT FROM 0000 UTC, 1 JANUARY 1984, FOR GUAYMAS, MEXICO (SEE FIG. 4) DEPICTING A SUPERADIABATIC LAYER BETWEEN 1000 AND 850 MB. DATA AND DELTAS (THE VALUE OF EACH DELTA IS SHOWN AT THE TOP OF EACH LAYER) ONLY SHOWN SURROUNDING THE SUPERADIABATIC LAYER.

LEV	PRES	HGHT	TEMP	DEWPT	DIR	SPD	DELTA
9	1013	12	228	8	305	11	
4	1000	123	310	90	305	13	-3
6	979	304	32767	32767	305	16	
6	944	609	32767	32767	305	9	
6	911	914	32767	32767	160	2	
6	879	1219	32767	32767	170	3	
5	859	1416	118	-182	32767	32767	
4	850	1503	124	-176	265	2	-27
5	841	1592	132	-168	32767	32767	
6	817	1828	32767	32767	325	3	
6	788	2133	32767	32767	295	6	
6	759	2438	32767	32767	290	12	
6	732	2743	32767	32767	285	14	
4	700	3111	38	-262	285	15	8

PRES: Pressure (mb)
 HGHT: Height (m)
 TEMP: Temperature (tenths Celsius)
 DEWPT: Dewpoint temperature (tenths Celsius)
 DIR: Wind direction (degrees)
 SPD: Wind speed (knots)

TABLE 15

DECODED GTS RAWINSONDE REPORT FROM 0000 UTC, 1 JANUARY 1981, FOR FORT NELSON, B.C., CANADA, ILLUSTRATING THREE CONSECUTIVE LARGE DELTAS FOR WHICH NO HYDROSTATIC CORRECTION COULD BE APPLIED. (VALUE FOR EACH DELTA SHOWN AT THE TOP FOR EACH LAYER).

LEV	PRES	HGHT	TEMP	DEWPT	DIR	SPD	DELTA
4	1000	274	32767	32767	32767	32767	
9	986	379	-221	-245	20	4	
4	850	1517	-3	-103	290	16	-7
4	700	3060	-57	-167	295	37	5
4	500	5630	-205	-315	315	52	7
4	400	7240	-325	-425	310	66	-2
4	300	2180	-489	32767	300	48	-7010
4	250	10580	-593	32767	300	54	7230
4	200	11740	-707	32767	300	58	-200
7	192	11980	-729	32767	300	58	
4	150	13460	-633	32767	295	54	-17
8	102	15859	32767	32767	290	69	
4	100	15960	-593	32767	290	68	-16

TABLE 16

GROSS OUT-OF-RANGE POINT ERROR CHECKS PERFORMED BY FSL
FOR PROCESSING RADIOSONDE DATA

Parameter	Acceptable Bounds
Pressure (mb)	0 < pres < 1085
Height (m)	-250 < hght < 25000
Temperature (C)	-90 < temp < 50

TABLE 17

SEGMENT OF THE PERIOD OF RECORD INVENTORY
(THE FULL INVENTORY IS SHOWN IN APPENDIX B.)

WBAN #	FROM			TO			NUMBER	#POSS	PERCENT
	DY	MO	YR	DY	MO	YR			
3109	11	AUG	1951	5	NOV	1955	1831	3095	59
3120	9	JUL	1957	31	OCT	1958	1878	8264	23
3121	18	APR	1957	28	SEP	1957	591	326	181
3123	21	JUL	1954	15	OCT	1954	192	173	111
3124	4	JAN	1955	30	JUL	1971	6571	12107	54
3125	1	JUL	1955	27	JUL	1971	7186	11742	61

TABLE 18

EXAMPLE FROM FULL RADIOSONDE INVENTORY FILE

3131	72290	SAN DIEGO MONTGOMERY			CA US	32.82	117.13	
		--- START ---			---- END ---			
		yr	mo	dy	yr	mo	dy	
							number	
1956		6	16		1980	4	5	17368
1980		4	7		1980	4	9	4
1980		4	11		1987	8	21	5355
1987		8	25		1987	8	25	2
1987		8	27		1987	9	4	18
1987		9	6		1988	1	2	233
1988		1	4		1989	1	3	722
1989		1	5		1989	1	20	30
1989		1	23		1989	3	29	130
1989		4	1		1989	6	7	132
1989		6	10		1989	6	13	8
1989		6	15		1989	6	18	6
1989		6	20		1989	7	27	75
1989		7	31		1989	8	31	62

TABLE 19

GENERAL FSL RADIOSONDE DATA BASE STATISTICS
(MAXIMUM NUMBER IN EACH COLUMN IS UNDERLINED.)

year	Max-snd	av-snd	max-lvl	av-lvl	num-snd	num-lns	size (MB)
1946	<u>16</u>	<u>9.4</u>	<u>22</u>	<u>18.4</u>	<u>6844</u>	<u>132867</u>	<u>2.13</u>
1947	<u>22</u>	<u>12.4</u>	<u>22</u>	<u>18.8</u>	<u>9045</u>	<u>169672</u>	<u>2.71</u>
1948	<u>100</u>	<u>84.7</u>	<u>36</u>	<u>21.5</u>	<u>61822</u>	<u>1327115</u>	<u>21.23</u>
1949	<u>113</u>	<u>94.9</u>	<u>35</u>	<u>21.4</u>	<u>69278</u>	<u>1483069</u>	<u>23.73</u>
1950	<u>129</u>	<u>112.4</u>	<u>39</u>	<u>22.1</u>	<u>82017</u>	<u>1811357</u>	<u>28.98</u>
1951	<u>137</u>	<u>127.3</u>	<u>41</u>	<u>22.9</u>	<u>92901</u>	<u>2129806</u>	<u>34.08</u>
1952	<u>149</u>	<u>132.2</u>	<u>44</u>	<u>24.1</u>	<u>94778</u>	<u>2326968</u>	<u>37.23</u>
1953	<u>170</u>	<u>150.5</u>	<u>41</u>	<u>25.4</u>	<u>109855</u>	<u>2785829</u>	<u>44.57</u>
1954	<u>166</u>	<u>145.0</u>	<u>45</u>	<u>25.6</u>	<u>105817</u>	<u>2712442</u>	<u>43.40</u>
1955	<u>181</u>	<u>156.8</u>	<u>42</u>	<u>25.8</u>	<u>114465</u>	<u>2952912</u>	<u>47.25</u>
1956	<u>186</u>	<u>166.4</u>	<u>39</u>	<u>26.6</u>	<u>121449</u>	<u>3229784</u>	<u>51.68</u>
1957	<u>199</u>	<u>169.0</u>	<u>41</u>	<u>28.4</u>	<u>123390</u>	<u>3204979</u>	<u>36.08</u>
1958	<u>171</u>	<u>148.2</u>	<u>43</u>	<u>29.0</u>	<u>108220</u>	<u>3138991</u>	<u>50.22</u>
1959	<u>167</u>	<u>145.0</u>	<u>48</u>	<u>29.5</u>	<u>105879</u>	<u>3127079</u>	<u>50.03</u>
1960	<u>168</u>	<u>140.8</u>	<u>45</u>	<u>29.6</u>	<u>102808</u>	<u>3046366</u>	<u>48.74</u>
1961	<u>169</u>	<u>142.9</u>	<u>43</u>	<u>27.7</u>	<u>104318</u>	<u>2888744</u>	<u>46.22</u>
1962	<u>166</u>	<u>151.0</u>	<u>44</u>	<u>27.7</u>	<u>110204</u>	<u>3054534</u>	<u>48.87</u>
1963	<u>169</u>	<u>150.6</u>	<u>42</u>	<u>27.7</u>	<u>109947</u>	<u>3044619</u>	<u>48.71</u>
1964	<u>174</u>	<u>153.6</u>	<u>44</u>	<u>27.9</u>	<u>112107</u>	<u>3125691</u>	<u>50.01</u>
1965	<u>175</u>	<u>153.3</u>	<u>46</u>	<u>27.9</u>	<u>111914</u>	<u>3125379</u>	<u>50.00</u>
1966	<u>171</u>	<u>151.9</u>	<u>44</u>	<u>28.2</u>	<u>110884</u>	<u>3125323</u>	<u>50.00</u>
1967	<u>168</u>	<u>151.4</u>	<u>53</u>	<u>30.7</u>	<u>110510</u>	<u>3392068</u>	<u>54.27</u>
1968	<u>170</u>	<u>151.1</u>	<u>48</u>	<u>30.8</u>	<u>110315</u>	<u>3394745</u>	<u>54.32</u>
1969	<u>167</u>	<u>149.9</u>	<u>67</u>	<u>32.7</u>	<u>109428</u>	<u>3583436</u>	<u>57.33</u>
1970	<u>171</u>	<u>143.6</u>	<u>69</u>	<u>34.9</u>	<u>104817</u>	<u>3656928</u>	<u>58.51</u>
1971	<u>173</u>	<u>144.2</u>	<u>67</u>	<u>36.9</u>	<u>105292</u>	<u>3882890</u>	<u>62.13</u>
1972	<u>142</u>	<u>135.7</u>	<u>69</u>	<u>39.4</u>	<u>99060</u>	<u>3905846</u>	<u>62.49</u>
1973	<u>155</u>	<u>138.8</u>	<u>87</u>	<u>40.0</u>	<u>101307</u>	<u>4053727</u>	<u>64.86</u>
1974	<u>158</u>	<u>141.4</u>	<u>85</u>	<u>40.3</u>	<u>103235</u>	<u>4163829</u>	<u>66.62</u>
1975	<u>175</u>	<u>146.9</u>	<u>81</u>	<u>40.4</u>	<u>107253</u>	<u>4336164</u>	<u>69.38</u>
1976	<u>166</u>	<u>147.2</u>	<u>80</u>	<u>41.3</u>	<u>107438</u>	<u>4437197</u>	<u>71.00</u>
1977	<u>181</u>	<u>147.6</u>	<u>80</u>	<u>42.1</u>	<u>107747</u>	<u>4535853</u>	<u>72.57</u>
1978	<u>182</u>	<u>147.4</u>	<u>81</u>	<u>40.7</u>	<u>107624</u>	<u>4375022</u>	<u>70.00</u>
1979	<u>225</u>	<u>145.4</u>	<u>75</u>	<u>41.0</u>	<u>106115</u>	<u>4350559</u>	<u>69.61</u>
1980	<u>174</u>	<u>141.6</u>	<u>81</u>	<u>41.6</u>	<u>105592</u>	<u>4502906</u>	<u>68.84</u>
1981	<u>164</u>	<u>139.9</u>	<u>78</u>	<u>42.6</u>	<u>102147</u>	<u>4354046</u>	<u>69.66</u>
1982	<u>159</u>	<u>136.8</u>	<u>77</u>	<u>43.3</u>	<u>99830</u>	<u>4325498</u>	<u>69.21</u>
1983	<u>154</u>	<u>136.7</u>	<u>84</u>	<u>43.5</u>	<u>99770</u>	<u>4345532</u>	<u>69.53</u>
1984	<u>182</u>	<u>135.9</u>	<u>84</u>	<u>43.9</u>	<u>99195</u>	<u>4353133</u>	<u>69.65</u>
1985	<u>180</u>	<u>138.8</u>	<u>83</u>	<u>43.8</u>	<u>101340</u>	<u>4439036</u>	<u>71.02</u>
1986	<u>260</u>	<u>137.1</u>	<u>91</u>	<u>43.3</u>	<u>100112</u>	<u>4331520</u>	<u>69.30</u>
1987	<u>146</u>	<u>133.3</u>	<u>90</u>	<u>42.6</u>	<u>97327</u>	<u>4149044</u>	<u>66.38</u>
1988	<u>123</u>	<u>104.4</u>	<u>87</u>	<u>40.9</u>	<u>76247</u>	<u>3118267</u>	<u>49.89</u>
1989	<u>172</u>	<u>119.7</u>	<u>88</u>	<u>45.3</u>	<u>87412</u>	<u>3956357</u>	<u>63.30</u>
1990	<u>152</u>	<u>122.4</u>	<u>91</u>	<u>47.4</u>	<u>89322</u>	<u>4233172</u>	<u>67.73</u>

Max-snd maximum number of soundings per time period
 av-snd average number of soundings per time period
 max-lv maximum number of levels for any sounding
 av-lv average number of levels per sounding
 num-snd total number of soundings for the year
 num-lns total number of lines for the year
 size size (MB) of the file for the year

TABLE 20

FSL RADIOSONDE DATA BASE STATISTICS SHOWING SOUNDING COMPLETENESS AND HYDROSTATIC QUALITY. VALUES ARE PERCENTAGES OF THE TOTAL OF NUMBER OF SOUNDINGS FOR EACH YEAR. (MAXIMUM VALUES IN EACH COLUMN ARE UNDERLINED.)

year	Sounding Completeness				Hydrostatic Balance			
	700MB	500MB	300MB	100MB	700MB	500MB	300MB	100MB
1946	<u>98.63</u>	92.14	73.71	17.31	80.76	75.61	59.66	<u>13.65</u>
1947	98.68	91.43	67.98	13.09	76.87	70.98	50.66	10.03
1948	99.70	97.32	89.49	34.20	91.47	89.09	82.13	<u>32.32</u>
1949	99.56	96.83	<u>88.63</u>	34.72	93.36	90.61	82.84	33.36
1950	99.79	97.44	90.84	48.75	94.06	91.65	85.24	46.31
1951	99.82	98.06	92.84	59.10	93.78	91.96	86.78	56.22
1952	99.79	97.85	92.74	66.43	94.32	92.23	87.01	62.74
1953	<u>99.86</u>	98.10	94.19	71.60	96.06	94.17	90.06	68.51
1954	99.91	98.71	95.70	74.69	97.04	95.63	92.27	71.79
1955	99.90	98.94	96.69	81.04	97.05	95.85	93.27	77.52
1956	99.90	98.79	96.46	82.01	96.78	95.49	92.80	78.12
1957	99.92	99.30	98.07	85.77	97.12	96.34	94.78	82.10
1958	99.93	99.57	98.96	91.01	96.05	95.45	94.51	86.18
1959	99.93	99.64	98.93	91.63	96.03	95.59	94.64	86.92
1960	99.94	99.76	99.27	93.34	96.32	96.06	95.34	88.85
1961	99.93	99.70	<u>98.35</u>	93.55	95.29	94.94	93.45	88.40
1962	99.88	99.69	99.13	94.23	96.61	96.34	95.71	90.48
1963	99.91	99.76	99.37	95.26	95.52	95.29	94.81	90.43
1964	99.85	99.57	99.17	95.53	95.52	95.21	94.76	91.16
1965	99.89	99.50	99.07	95.76	97.04	96.69	96.20	92.87
1966	99.94	99.60	99.18	95.91	97.43	97.23	96.77	93.44
1967	<u>99.92</u>	99.74	99.18	95.67	97.57	97.35	96.75	93.22
1968	<u>99.95</u>	99.72	99.10	95.71	97.71	97.43	96.71	93.35
1969	<u>99.90</u>	98.44	98.14	94.72	98.05	96.54	96.15	92.68
1970	99.84	97.48	96.96	93.82	98.88	96.51	95.91	92.69
1971	99.81	95.08	94.60	90.82	98.88	94.15	93.60	89.78
1972	<u>99.95</u>	99.69	99.38	95.18	98.95	98.65	98.29	94.00
1973	99.92	99.42	98.18	93.58	98.93	98.40	97.14	92.49
1974	99.94	99.36	98.06	93.72	99.02	98.41	97.07	92.67
1975	99.90	97.03	95.70	91.51	99.05	96.16	94.80	90.58
1976	99.91	97.72	96.63	92.63	99.07	96.86	95.73	91.71
1977	99.85	97.87	96.71	92.38	99.06	97.04	95.86	91.47
1978	99.88	97.80	96.50	92.29	99.03	96.97	95.64	91.43
1979	99.90	98.25	96.50	92.76	99.10	97.42	95.65	91.87
1980	99.95	99.59	97.51	93.69	99.09	98.69	96.56	92.63
1981	<u>99.92</u>	99.77	98.56	95.00	98.58	97.81	96.53	92.73
1982	99.92	99.78	98.47	94.96	99.19	98.98	97.59	93.87
1983	99.95	<u>99.85</u>	98.56	95.30	99.19	99.00	97.65	94.22
1984	<u>99.95</u>	99.84	98.76	<u>95.77</u>	99.31	99.12	97.99	<u>94.80</u>
1985	99.94	99.84	98.50	95.20	99.39	99.21	97.83	94.43
1986	99.91	99.72	97.94	93.40	99.26	99.02	97.17	92.51
1987	99.92	99.69	96.84	91.52	99.33	99.02	96.13	90.71
1988	99.93	99.64	96.65	89.66	<u>99.75</u>	<u>99.39</u>	96.35	89.30
1989	99.83	99.60	96.94	90.60	98.31	97.80	94.67	87.61
1990	99.85	99.59	98.39	93.23	96.91	96.36	94.53	88.74

TABLE 21

DESCRIPTION OF THE FSL RADIOSONDE STATION
HISTORICAL FILE

Column #	description
2-4	3-letter identifier
6-10	WBAN number
12-16	WMO number
18-23	latitude (deg.min)
25-30	longitude (deg.min)
32-35	elevation (m)
38-43	beginning date (yyymmdd)
45-50	ending date (yyymmdd)
53-76	station name
78-79	state/province abbreviation
81-82	country abbreviation (see below)
88-92	previous (from) WBAN station number
94-98	next (to) WBAN station number
100-104	cross reference WBAN number
106	wind only (Pibal) identifier
108-132	remarks

Country codes:

US: United States	JA: Jamaica
CN: Canada	HO: Honduras
MX: Mexico	CI: Cayman Islands
PN: Panama	GU: Guatemala
BA: Barbados	CU: Cuba
AN: Antigua	BM: Bahamas
GU: Guadeloupe	BI: British West Indies
NA: Netherland Antilles	BE: Bermuda
SL: St Lucia	TR: Trinidad
DR: Dominican Republic	

TABLE 22

DESCRIPTION OF THE FSL RADIOSONDE EQUIPMENT
HISTORICAL FILE

Column #	Description
2-4	3-letter identifier
6-10	WBAN number
12-16	WMO number
18-19	number of entries to follow

Each entry contains a date (yymmdd) indicating the type of instrument, radiosonde, computer technology, etc. (code, see below) used on the date specified.

Equipment code

Ground Equipment:

G0: 72.2 equipment
 G1: SCR 584
 G2: SCR 658 (and Canadian METOX)
 G3: GMD-1
 G4: GMD-1A
 G5: GMD-1B
 G6: GMD-4
 G7: WBRT-57
 G8: WBRT-60
 G9: LORAN

Humidity Sensors:

H1: carbon hygistor
 H2: Lithium Chloride hygistor
 H3: redesigned duct
 H4: new carbon hygistor

Computer technology:

C1: transistorized equipment
 C2: time share computer operation
 C3: mini-computer
 C4: ART operation
 C5: mini-ART 1
 C6: mini-ART 2
 C7: micro-ART

Radiosonde:

S1: hyposometer (pressure)
 S2: transponder type
 S3: accu-lock sonde
 S4: VIS B sonde
 S5: SDC sonde

Miscellaneous:

M1: relative humidity to dewpoint
 M2: ms-1 to knots
 M3: contract personnel

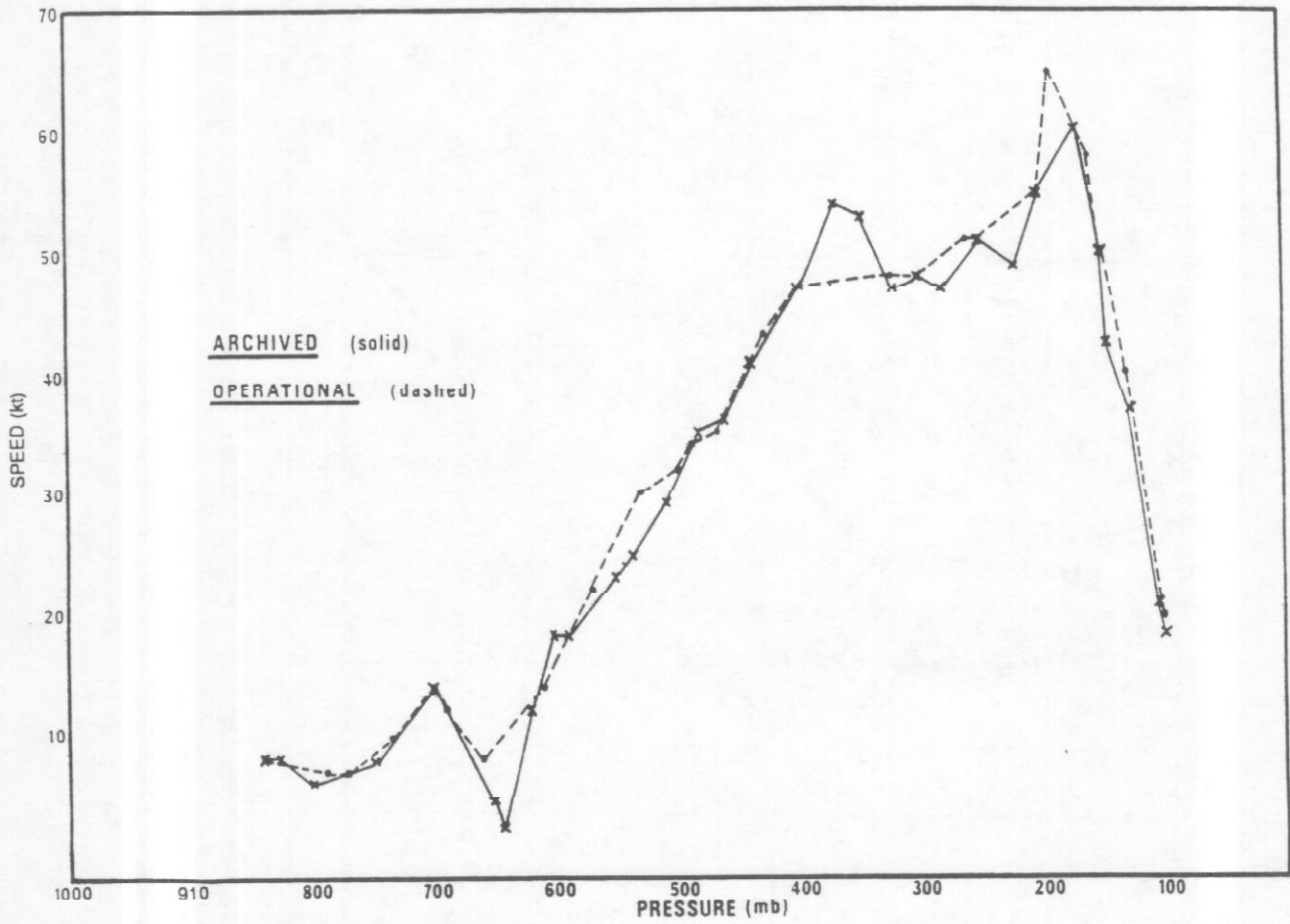


Fig. 1 Comparison of GTS and NCDC-processed wind speed versus pressure for the Oklahoma City, OK, sounding taken on 11 May 1985.

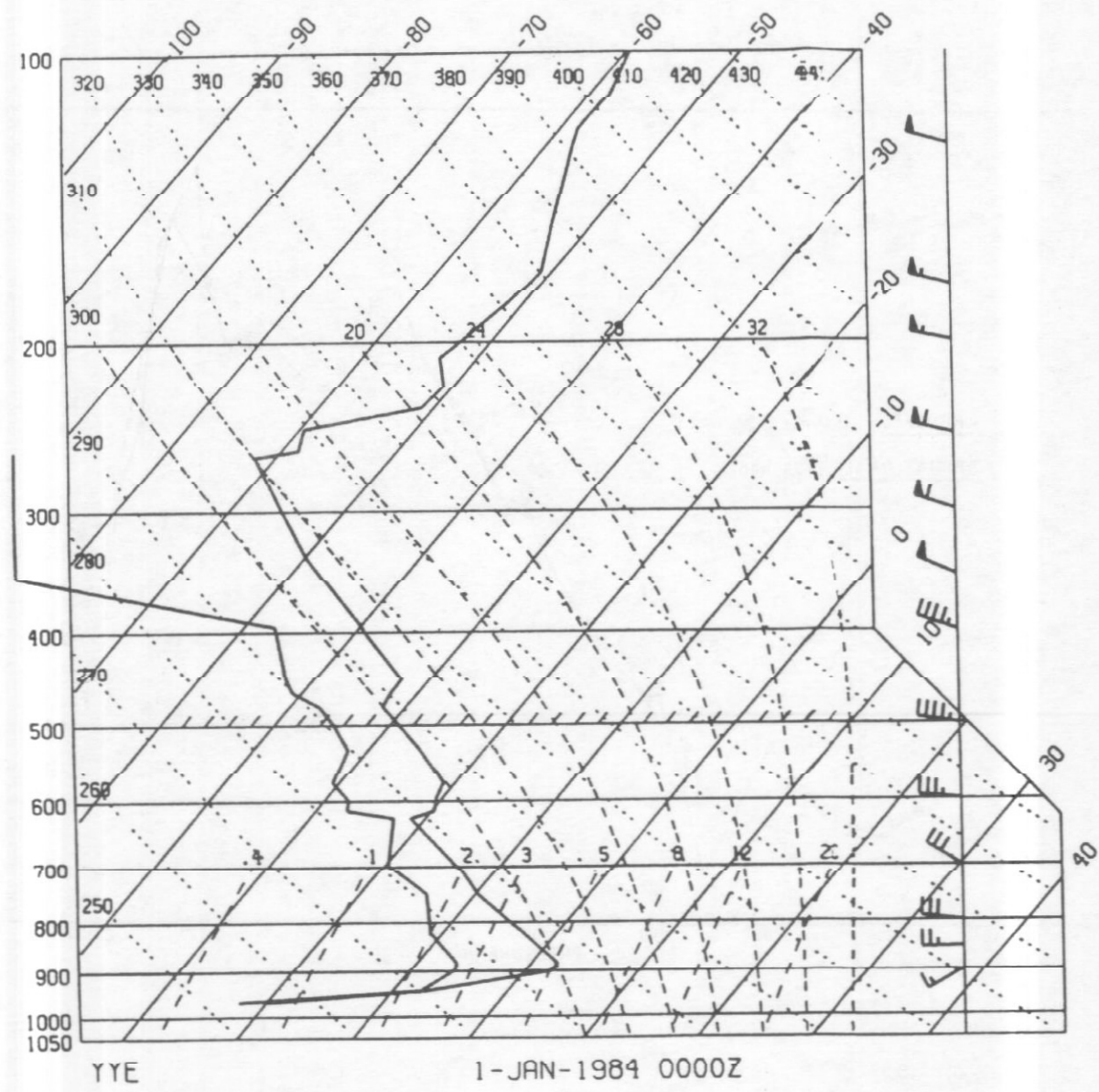


Fig. 2 Skew-T, log-P plot of the sounding taken at Fort Nelson, British Columbia, Canada, on 1 January 1984.

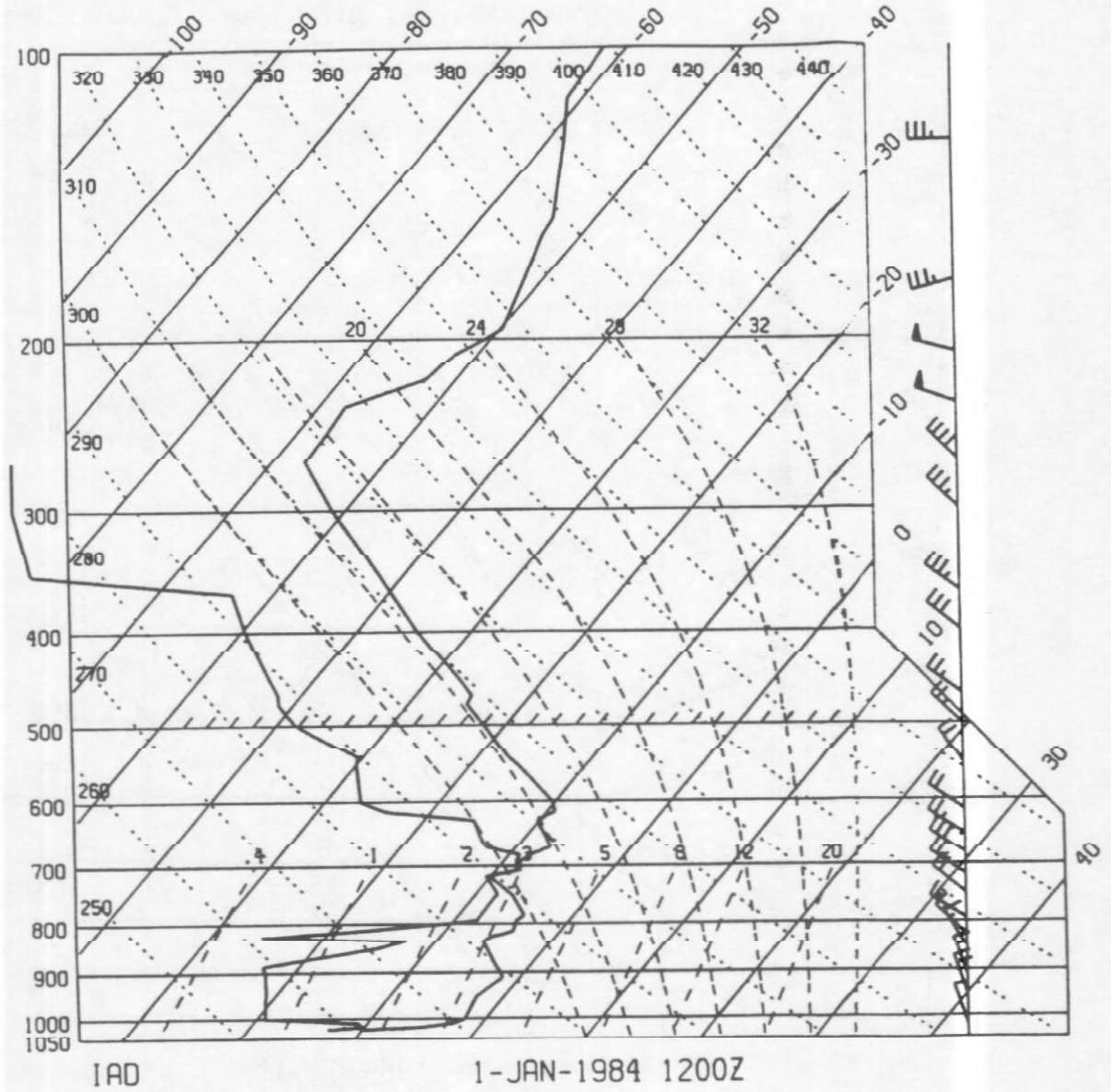


Fig. 3 Same as Fig. 2, except for Washington, D.C. (Dulles).

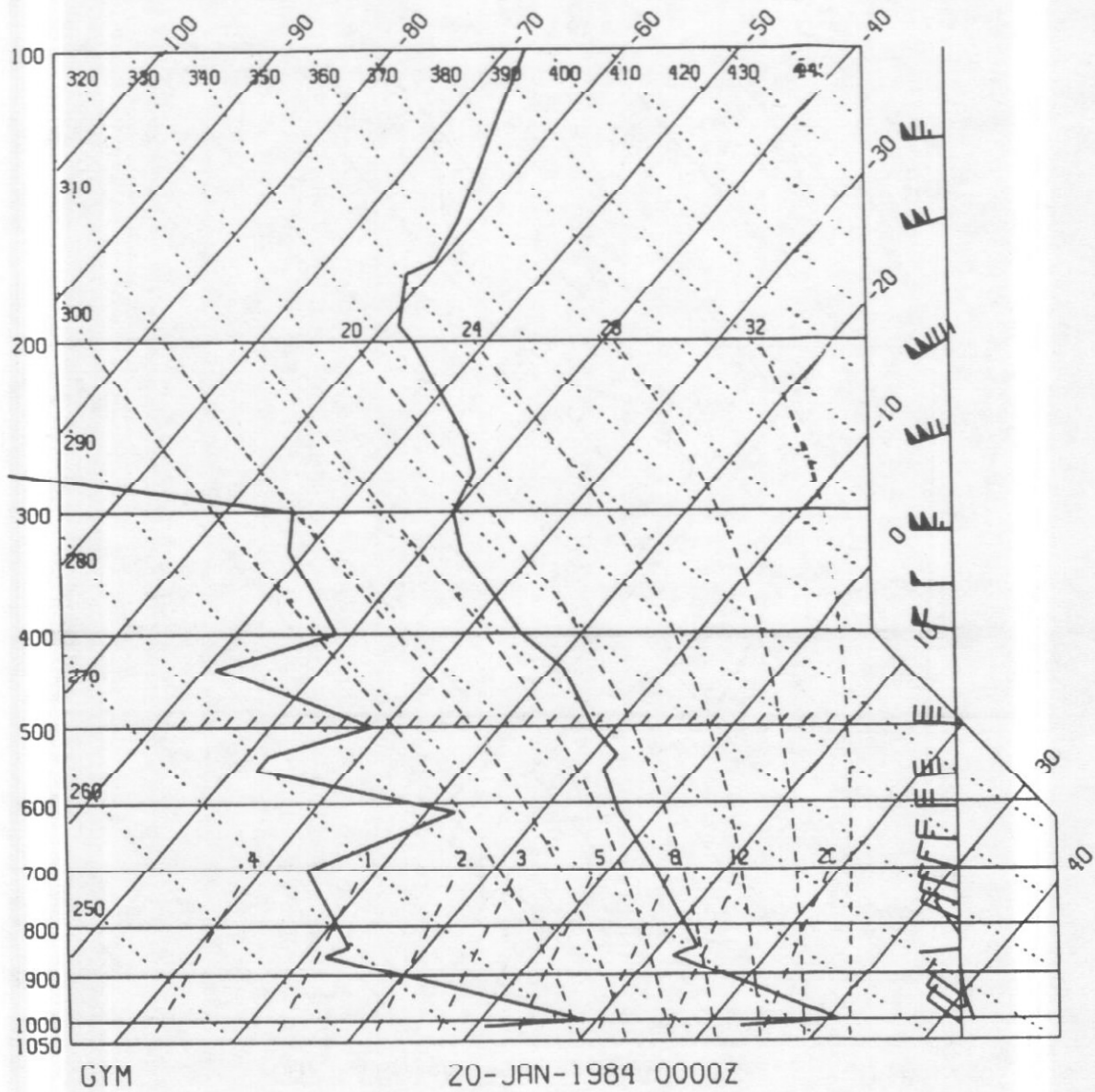


Fig. 4 Same as Fig. 2, except for Guaymas, Mexico, on 20 January 1984.

FSL Rawinsonde Data Format

FSL Rawinsonde data format

The official FSL data format is similar to the format used by the National Severe Storms Forecast Center (NSSFC) in Kansas City. When a user of the data base retrieves data using the direct access method discussed in section 7, data appears in this ascii "card image" format. The first 4 lines of the sounding are identification and information lines. All additional lines are data lines. An entry of 32767 indicates that the information is either missing, not reported, or not applicable.

---COLUMN NUMBER---

1	2	3	4	5	6	7
LINTYP			header lines			
254	YEAR	MONTH	DAY	TIME		
1	WBAN#	TRCPL	WMO#	LINE	ELEV	RTIME
2	HYDRO	(blank)	MAXW	LINE	INDEX	SOURCE
3	(blank)		STAI	(blank)	SONDE	WSUNITS
	PRESSURE	HEIGHT	data lines	DEWPT	WIND DIR	WIND SPD
9			TEMP			
4						
5						
6						
7						
8						

LEGEND

- LINTYP: type of identification line
 254=indicates a new sounding in the output file
 1=station identification line
 2=sounding checks line
 3=station identifier and other indicators line
 4=surface level
 5=mandatory level
 6=significant level
 7=wind level (PPBB) (GTS or merged data)
 8=tropopause level (GTS or merged data)
 9=maximum wind level (GTS or merged data)
 time of report in UTC
 HOUR: latitude in degrees and hundredths
 LAT: longitude in degrees and hundredths
 LON: elevation from station history in meters
 ELEV: is the actual release time of radiosonde from TTBB. Appears in GTS data only.
 RTIME: the pressure of the level to where the sounding passes the hydrostatic check (see section 4.3)**
 HYDRO: the pressure of the level having the maximum wind in the sounding. If within the body of the sounding there is no "8" level then MXNN is estimated (see section 3.2).
 MXWD: the pressure of the level containing the tropopause. If within the body of the sounding there is no "7" level, then "PROPL is estimated (see section 3.3)**
 TROPI: number of levels in the sounding, including the 4 identification lines.
 LINES: indicator for estimated tropopause. A "7" indicates that sufficient data was available to attempt the estimation; 11 indicates that data terminated and that tropopause is a "suspected" tropopause.
 TINDEX: 0=data acquired from NCDC(NCAR) or AES only
 SOURCE: 1=NSSFC GTS or FSL GTS data only
 2=merge of NCDC and GTS data
 SONDE: type of radiosonde code from TTBB. Only reported with GTS data
 10=VIZ "A" type radiosonde
 11=VIZ "B" type radiosonde
 12=Space data corp.(SDC) radiosonde.

WSUNITS:wind speed units (selected upon output)
 0-meters per second
 1-knots

PRESSURE: in whole millibars (mb)
 HEIGHT: height in meters (m)
 TEMP: temperature in tenths of degrees Celsius
 DEWPT: dew point temperature in tenths of a degree Celsius
 WIND DIR: wind direction in degrees
 WIND SPD: wind speed in either knots or tenths of a meter per second (selected by user upon output)

An example of fortran format statements necessary to read output rawinsonde data, according to LINTYP, is as follows:

```
LINTYP
254      (3i7, 6x, a4, i7)
1        (3i7, 2f7.2, 2i7)
2        (7i7)
3        (i7, 3x, a10)
4, 5, 6, 7, 8, 9  (7i7)
```

** Refer to the sections in this Technical Memorandum.

APPENDIX B(1)

Record Inventory for North American Upper-air Stations

WBAN	WMO	Period of record inventory for North America upper-air stations	START	END	1951	1952	1953	1954	1955	1956	1957	1958	1959	1960	1961	1962	1963	1964	1965	1966	1967	1968	1969	1970	1971	1972
3109	72387	MERCURY/TEST SITE	8	11	1955	11	5																			
3120	72388	N CHINA LAKE/B-1 RANGE	7	9	1958	10	31																			
3121	99999	ST GEORGE	4	18	1957	9	28																			
3122	72282	CAMP PENDLETON	7	21	1954	10	15																			
3124	72273	FT HUACHUCA	1	4	1971	7	30																			
3125	72280	FUMA	7	1	1971	7	27																			
3131	72280	SAN DIEGO MONTGOMERY	6	16	1989	8	31																			
3132	72485	TOMOPAH	9	20	1958	10	31																			
3133	72385	FUCCA FLAT	9	16	1979	5	14																			
3134	99999	BAKER	4	23	1957	9	28																			
3143	72385	JACKASS FLATS	4	29	1967	12	19																			
3146	72281	EL CENTRO	2	28	1968	8	30																			
3149	72278	PHOENIX/LITCHFIELD PARK	8	26	1963	10	22																			
3158	72291	SAN NICOLAS/SITE #2	4	6	1983	1	7																			
3160	72387	DESERT ROCK/MERCURY	5	16	1990	9	26																			
3160	72293	KIRAMAR	9	22	1990	9	26																			
3816	72435	PAUCUHA	12	5	1990	6	26																			
3851	72326	KNOXVILLE/McGHEE-TYSON	2	15	1956	6	14																			
3855	72222	PENSACOLA/F. SHERMAN FLD	6	16	1988	9	25																			
3860	72453	SALEM	10	1	1988	11	28																			
3879	72229	CENTREVILLE	11	16	1990	9	26																			
3881	72344	FT SMITH	3	17	1964	5	18																			
3926	72344	LAKE CHARLES	3	17	1964	5	18																			
3937	72230	JACKSON/THOMPSON FLD	7	1	1990	9	26																			
3940	72245	JACKSON/THOMPSON FLD	7	1	1990	9	26																			
3946	72349	KONETT	9	5	1990	9	26																			
3948	72357	NORMAN	1	1	1990	9	26																			
3951	72247	LONGVIEW	7	13	1990	9	26																			
3952	72340	N LITTLE ROCK	12	20	1990	9	26																			
4734	71722	MANIWAKI	7	1	1990	9	26																			
4738	72528	NIAGARA FALLS	3	15	1960	8	20																			
10701	78806	BALBOA/ALBROOK AFB	1	1	1990	9	26																			
10717	80222	KOGETA	8	17	1971	12	31																			
10809	78762	SAN JOSE/JUAN SANTA MARIA	6	1	1990	9	26																			
11501	78954	SEAWELL APT	1	30	1990	9	26																			
11621	78967	TRINIDAD NAS	2	1	1969	12	8																			
11629	78486	SANTO DOMINGO	8	6	1990	6	22																			
11630	78535	ROOSEVELT ROADS	10	1	1988	12	7																			
11631	78526	SAN JUAN	1	1	1950	1	31																			
11634	78970	TRINIDAD/PIARCO IAP	12	12	1990	9	26																			
11636	78526	SAN JUAN/ISLA GRANDE	2	1	1955	5	23																			
11641	78526	SAN JUAN/ISLA VERDE	5	24	1990	9	26																			
11642	78897	POINT A PITRE/RAIZET	2	21	1990	9	26																			
11643	78988	CURACAO/WILLEMSTAD	6	5	1990	9	26																			
11644	78949	ST LUCIA AFB	7	20	1957	10	3																			
11645	78666	SINT MAARTEN/JULIANA	10	2	1990	9	26																			
11646	78467	SABANA DE LA MAR	9	19	1962	8	4																			
11647	78861	ST JOHN/COLLIDGE AFB	9	1	1989	5	1																			
11706	78367	GUANTANAMO NAS	8	1	1990	9	25																			
11715	78397	KINGSTON/PALISADOES	9	4	1990	9	26																			
11807	78501	SWAN ISLAND/ISLAS DEL CIS	8	7	1980	2	6																			
11813	78384	GRAND CAYMAN	8	14	1990	9	26																			
11816	78724	CHOLUETCA	1	17	1975	12	23																			
11817	78720	TEGUCIGALAPA D.C.	6	3	1990	9	26																			
11818	78583	BELIZE	6	1	1990	9	26																			
11901	78641	GUATEMALA CITY	11	8	1989	2	19																			
11903	76679	MEXICO CITY/TACUYA	1	1	1990	9	26																			
11904	76692	VERACRUZ	1	25	1990	9	26																			
12711	78355	CAMAGUAY	4	14	1990	9	18																			
12712	78063	GRAND BAHAMA/GOLD ROCK CK	1	25	1970	5	29																			

APPENDIX B(1) (Continued)

Record Inventory for North American Upper-air Stations

110050	72408 PHILADELPHIA (EMSU)	1969	6	17	1977	5	18
110052	72408 PHILADELPHIA (EMSU)	1970	8	11	1970	11	10
110053	72408 PHILADELPHIA (EMSU)	1970	7	13	1971	9	2
110060	72524 CLEVELAND (EMSU)	1971	4	1	1971	12	30
110070	72423 LOUISVILLE (EMSU)	1971	4	3	1971	12	30
110080	74530 DENVER (EMSU)	1971	4	23	1971	12	30
110090	74704 EL MONTE (EMSU)	1971	4	1	1979	9	28
110100	72295 LOS ANGELES (EMSU)	1971	5	1	1979	9	30
110110	74505 SAN JOSE (EMSU)	1971	8	10	1971	12	30
110111	74505 SAN JOSE/BRENTWOOD (EMS)	1972	6	19	1972	6	23
110112	74505 SAN JOSE/SANTA ROSA (EMS)	1972	9	6	1972	9	8
110110	72509 BOSTON (EMSU)	1971	8	24	1971	12	30
110110	72243 HOUSTON (EMSU)	1971	8	16	1979	6	29
110110	72793 SEATTLE (EMSU)	1971	10	18	1971	12	30
110111	72793 SEATTLE/BOEING FLD (EMSU)	1971	9	15	1971	10	14
110150	74479 PITTSBURGH (EMSU)	1971	11	15	1971	12	30
110170	72414 CHARLESTON (EMSU)	1975	1	2	1979	11	29
110180	72228 BIRMINGHAM (EMSU)	1975	1	2			

Station History for North American Upper-air Stations

3109	72387	36.56	116.04	1259	510811	520428	MERCURY/TEST SITE	NV US		
3109	72387	36.36	115.58	1155	520429	521204	MERCURY/TEST SITE	NV US		
3109	72387	36.57	116.03	1197	521204	530605	MERCURY/TEST SITE	NV US	3133	
3109	72387	36.57	116.05	1196	552021	551165	MERCURY/TEST SITE	NV US		
3120	72388	35.47	117.47	687	470709	540309	N CHINA LAKE/B-1 RANGE	CA US		
3120	72388	35.47	117.47	670	540310	541231	N CHINA LAKE/G-1 RANGE	CA US		
3120	72388	35.47	117.47	666	570101	640229	N CHINA LAKE/G-1 RANGE	CA US	93104	
3121	99999	37.06	113.36	895	570417	570928	ST GEORGE	UT US		
3121	99999	37.06	113.36	895	540721	541015	CAMP FENDLETON	CA US		
3124	72273	31.34	110.20	1425	550104	550108	FT HUACHUCA	AZ US		inter obs throughout
3124	72273	31.34	110.20	1428	550109	580611	FT HUACHUCA	AZ US		
3124	72273	31.34	110.20	1420	580612	580617	FT HUACHUCA	AZ US		
3124	72273	31.34	110.20	1422	580618	590226	FT HUACHUCA	AZ US		
3124	72273	31.34	110.20	1423	590227	590325	FT HUACHUCA	AZ US		
3124	72273	31.34	110.20	1432	590326	611028	FT HUACHUCA	AZ US		
3124	72273	31.34	110.20	1439	611029		FT HUACHUCA	AZ US		
3125	72280	32.51	114.24	106	540511	560831	YUMA	AZ US		
3125	72280	32.50	114.24	106	560901	580917	YUMA	AZ US		
3125	72280	32.52	114.20	131	580918	610906	YUMA	AZ US		
3125	72280	32.52	114.20	98	610907	630607	YUMA	AZ US		
3125	72280	32.50	114.24	98	630608	630630	YUMA	AZ US		
3125	72280	32.52	114.20	131	650601	710727?	YUMA/US ARMY MET TEAM	AZ US		
3131	72290	32.49	117.08	124	560616	8909.3	SAN DIEGO MONTGOMERY	CA US	93112	NO SAN DIEGO 08 9/14/90!
3132	72485	38.04	117.06	1650	560920	581031	TONOPAH	NV US	23128	
3133	72385	36.57	116.03	1196	560916	590428	YUCCA FLAT	NV US	3109	
3133	72385	36.57	116.03	1196	590815	6007.4	YUCCA FLAT	NV US	3143	
3133	72385	36.57	116.03	1196	610914	660920	YUCCA FLAT	NV US	3143	
3133	72385	36.57	116.03	1196	609221	6811.0	YUCCA FLAT	NV US		
3133	72385	36.57	116.03	1198	68.111	790514	YUCCA FLAT	NV US		
3134	99999	35.16	116.05	284	570423	570928	BAKER	CA US	23169	
3143	72385	36.48	116.16	1100	590429	590815	JACKASS FLATS	CA US	3133	
3143	72385	36.48	116.16	1100	600526	610420	JACKASS FLATS	NV US	3133	
3143	72385	36.48	116.16	1102	610421	671219	JACKASS FLATS	NV US		
3146	72281	32.58	115.49	73	620228	680830	EL CENTRO	CA US		
3148	74724	32.57	112.40	262	999999		GILA BEND AAF	AZ US	23183	
3149	72278	33.26	112.22	295	630813	631022	PHOENIX/LITCHFIELD PARK	AZ US		
3158	72291	33.16	119.33	9	730901	830107	SAN NICOLAS/SITE #2	CA US	93116	2 SITES USED
3176	72387	36.37	116.01	1007	780516		DESERT ROVER/MERCURY	NV US	3133	
3176	72387	35.20	117.06	962?	999999		SUPERIOR VALLEY GUN RANGE/CA US			
3182	74611	35.17	116.37	716?	999999		BICYCLE LAKE AAF	CA US		
3190	72293	32.52	117.09	147	890913		MIRAMAR NAS	CA US	3131	
3816	72435	37.04	88.46	126	881128		PADUCAH	KY US	3879	
3851	72326	35.49	83.59	301	550215	560618	KNOXVILLE/MCGHEE-TYSON	TN US	93829	
3855	72222	30.21	87.19	10	550523	680630	PENSACOLA/F. SEERMAN FLD	FL US	93818	
3860	72425	38.22	82.33	246	611201		HUNTINGTON	WV US		
3879	72433	38.19	88.58	174	690625	700130	SALEM	IL US	3816	
3879	72433	38.19	88.58	175	700131	881128	SALEM	IL US		
3881	72229	32.54	87.15	140	741116		CENTERVILLE	AL US	13895	
3926	72344	35.20	94.18	146	530317	550930	FT SMITH	AR US		
3926	72344	35.18	94.19	147	560215	560630	FT SMITH	AR US		
3926	72344	35.20	94.22	140	570201	570831	FT SMITH	AR US		
3926	72344	35.18	94.18	146	580201	581031	FT SMITH	AR US		
3926	72344	35.19	94.16	142	590201	640518	FT SMITH	AR US		
3937	72340	30.07	93.13	5	611231		LAKE CHARLES	LA US	13941	
3940	72235	32.19	90.05	100	681018	780917	JACKSON/THOMPSON FLD	MS US	13956	archive mis 2 yrs
3940	72235	32.19	90.04	91	780918		JACKSON/THOMPSON FLD	MS US		
3946	72349	36.53	93.54	438	709905		MORETT	MO US	13983	
3948	72357?	35.14	97.28	362	740101	750106	NORMAN	OK US	13919	13967
3948	72357	35.14	97.28	362	890328		NORMAN	OK US	13967	
3951	72247	32.21	94.39	124	750713		LONGVIEW	TX US	13957	
3952	72340	34.50	92.16	172	751219		N LITTLE ROCK	AR US	13963	
4734	72722	46.23	75.58	170	530701	770701	MANIWAKI	PQ CN		
4734	71722	46.23	75.58	170	770701		MANIWAKI	PQ CN		
4738	72528	43.07	78.55	182	540315	600820	NIAGARA FALLS	NY US		
4740	99999?	43.59	77.09	98?	601199	610439	PICTON	ON CN	14733	14733
10701	78806	8.59	79.56	66	431199		BALBOA/ALBROOK AFB	ON CN		no data in archive

Station History for North American Upper-air Stations

CBO 10717	80222	4.42	74.09	2547	600817	630317	BOGOTA	BOGOTA	CO	
CBO 10717	80222	4.42	74.09	2541	630318		BOGOTA	BOGOTA	CO	
ROL 10809	78162	9.59	84.13	0	830601		SAN JOSE/JUAN SANTA MARIA	SAN JOSE/JUAN SANTA MARIA	CR	
BDI 11501	78954	13.04	59.30	56	650130	711026	SEAWELL APT	SEAWELL APT	BA	
BDI 11501	78954	13.04	59.30	47	711027		SEAWELL APT	SEAWELL APT	BA	
ANU 11608	78861	17.07	61.47	4	440199	490720	ST JOHNS/COOLIDGE AAFB	ST JOHNS/COOLIDGE AAFB	AN	11647
CGU 11610	78967	10.35	66.06	6	440505	451209?	SAN JUAN	SAN JUAN	PR	11631
CGU 11621	78967	10.41	61.37	21	420501	490430	TRINIDAD NAS	TRINIDAD/WALLER FLD	TR	11621
CGU 11621	78967	10.41	61.37	21	500101	501031	TRINIDAD NAS	TRINIDAD NAS	TR	11610
CGU 11621	78967	10.41	61.37	18	501101	520831	TRINIDAD NAS	TRINIDAD NAS	TR	
CGU 11621	78967	10.41	61.37	2	520901	670615	TRINIDAD NAS	TRINIDAD NAS	TR	
CGU 11621	78967	10.41	61.37	2	670616	691208	TRINIDAD/CHAGUARAMAS	TRINIDAD/CHAGUARAMAS	TR	11634
SDQ 11629	78486	18.28	69.53	14	620806		SANTO DOMINGO	SANTO DOMINGO	DR	11646
JNR 11630	78335	18.15	65.34	20	881001	881207	ROOSEVELT ROADS	ROOSEVELT ROADS	PR	11608
?	11631	78326	18.27	66.06	6	451210	491108	SAN JUAN	PR	11636
?	11631	78326	18.28	66.07	6	491109	500113	SAN JUAN	PR	11621
KPP 11634	78970	10.35	61.21	12	691212		TRINIDAD/PIARCO IAP	TRINIDAD/PIARCO IAP	TR	11631
SIG 11636	78526	18.27	66.06	19	502021	560210	SAN JUAN/ISLA GRANDE	SAN JUAN/ISLA GRANDE	PR	11641
JSJ 11641	78526	18.26	66.00	23	550701	560331	SAN JUAN/ISLA VERDE	SAN JUAN/ISLA VERDE	PR	
JSJ 11641	78526	18.26	66.00	19	560210	550630	SAN JUAN/ISLA VERDE	SAN JUAN/ISLA VERDE	PR	
JSJ 11641	78526	18.26	66.00	6	560401	750223	SAN JUAN/ISLA VERDE	SAN JUAN/ISLA VERDE	PR	
JSJ 11641	78526	18.26	66.00	3	750224		SAN JUAN/ISLA VERDE	SAN JUAN/ISLA VERDE	PR	
FFR 11642	78997	16.16	61.32	8	560221	590430	POINT A PITRE/RAIZET	POINT A PITRE/RAIZET	GU	
FFR 11642	78997	16.16	61.31	8	590301	721231	POINT A PITRE/RAIZET	POINT A PITRE/RAIZET	GU	
ACC 11643	78988	12.11	68.58	8	890101		CURACAO/WILLEMSTAD	CURACAO/WILLEMSTAD	NA	
ACC 11643	78988	12.11	68.58	9	610312	700521	CURACAO/WILLEMSTAD	CURACAO/WILLEMSTAD	NA	
ACC 11643	78988	12.12	68.58	9	700522	760522	CURACAO/WILLEMSTAD	CURACAO/WILLEMSTAD	NA	
ACC 11643	78988	12.12	68.58	54	760523		CURACAO/WILLEMSTAD	CURACAO/WILLEMSTAD	NA	
SLU 11644	78949	13.45	60.59	30	560720	571099	ST LUCIA AAFB	ST LUCIA AAFB	SL	
ACM 11645	78866	18.02	63.07	3	561902	660628	SINT MAARTEN/JULIANA	SINT MAARTEN/JULIANA	NA	
ACM 11645	78866	18.01	63.07	3	660629		SINT MARTIN/JULIANA	SINT MARTIN/JULIANA	NA	
ACM 11645	78866	18.01	63.07	3	660629		SINT MARTIN/JULIANA	SINT MARTIN/JULIANA	NA	
SDM 11646	78467	19.01	69.23	11	560919	620804	SABANA DE LA MAR	SABANA DE LA MAR	DR	
KPA 11647	78861	17.07	61.47	4	570901	890501	SABANA DE LA MAR	SABANA DE LA MAR	DR	11629
KJP 11704	78197	17.53	77.18	34	431099	490920	ST JOHN/COOLIDGE AAFB	ST JOHN/COOLIDGE AAFB	AN	11604
UGM 11706	78167	19.54	75.09	20	460801	520731	KINGSTON/VERNON FLD	KINGSTON/VERNON FLD	JA	
UGM 11706	78167	19.54	75.09	16	520801	550228	GUANTANAMO NAS	GUANTANAMO NAS	CU	
UGM 11706	78167	19.54	75.09	29	550301	660113	GUANTANAMO NAS	GUANTANAMO NAS	CU	
UGM 11706	78167	19.54	75.09	32	660114	760630	GUANTANAMO NAS	GUANTANAMO NAS	CU	
UGM 11706	78167	19.54	75.09	6	760701		GUANTANAMO NAS	GUANTANAMO NAS	CU	
KJP 11715	78197	17.56	76.47	7	560903	630514	KINGSTON/PALISADOES	KINGSTON/PALISADOES	JA	11704
KJP 11715	78197	17.56	76.47	1	630515		KINGSTON/PALISADOES	KINGSTON/PALISADOES	JA	
SWA 11807	78501	17.21	83.56	10	390720	600419	SWAN ISLAND/ISLAS DEL CISNE	SWAN ISLAND/ISLAS DEL CISNE	HO	
SWA 11807	78501	17.21	83.56	11	600420	610116	SWAN ISLAND/ISLAS DEL CISNE	SWAN ISLAND/ISLAS DEL CISNE	HO	
KCR 11813	78184	19.18	81.22	10	610117	800206	SWAN ISLAND/ISLAS DEL CISNE	SWAN ISLAND/ISLAS DEL CISNE	HO	
HTC 11817	78120	14.02	87.11	49	730117	751223	GRAND CAYMAN	GRAND CAYMAN	CI	
ZBZ 11818	78383	17.32	88.18	5	820801		CHOLSTECA	CHOLSTECA	HN	
GUA 11901	78641	14.32	90.34	1496	731108	890219	TEGUCIGALAPA, D. C.	TEGUCIGALAPA, D. C.	HO	
MEX 11903	76679	19.24	99.12	2306	430210	671212	BELIZE	BELIZE	BE	
MEX 11903	76679	19.25	99.05	2234	671213	700820	GUATEMALA CITY	GUATEMALA CITY	GU	
MEX 11903	76679	19.26	99.04	2234	700821		MEXICO CITY/INT APT	MEXICO CITY/INT APT	MX	
VER 11904	76692	19.11	96.07	12	520125	521215	MEXICO CITY/INT APT	MEXICO CITY/INT APT	MX	12948
VER 11904	76692	19.11	96.07	13	521216	640228	VERACRUZ	VERACRUZ	MX	
CMW 12711	78155	21.25	77.52	122	480101	601031	VERACRUZ	VERACRUZ	MX	
CMW 12711	78155	21.25	77.52	122?	890101		CAMAGUAY	CAMAGUAY	CU	
YGM 12712	78063	26.37	78.22	6	510125	701216	GRAND BAHAMA/GOLD ROCK CK	GRAND BAHAMA/GOLD ROCK CK	BM	
YEM 12713	78076	25.16	76.18	26	520215	570699	ELEUTHERA I/COFFIN HILLS AA	ELEUTHERA I/COFFIN HILLS AA	BM	
YEM 12713	78076	25.16	76.18	25	570799	631299	ELEUTHERA I/COFFIN HILLS AA	ELEUTHERA I/COFFIN HILLS AA	BM	
YEM 12713	78076	25.16	76.18	27	640199	701217	ELEUTHERA I/COFFIN HILLS AA	ELEUTHERA I/COFFIN HILLS AA	BM	
KJT 12714	78118	21.27	71.09	9	541116	830622	GRAND TURK IS AFB	GRAND TURK IS AFB	BM	
12715	78107	22.22	73.02	21	551110	571002	FLAMINGO HILL/MAYAGUAN AAFB	FLAMINGO HILL/MAYAGUAN AAFB	BI	
YSM 12716	78989	24.01	74.31	5	560112	641215	SAN SALVADOR AAFB/BONEFISH	SAN SALVADOR AAFB/BONEFISH	BM	

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Station History for North American Upper-air Stations

NGU	13750	72308	36.56	76.17	6	521116	551115	NORFOLK	VA US	13737
NDY	13760	74574	38.20	77.01	30	451001	560202	DAHLGREN	VA US	
CUN	13801	72226	32.25	86.14	53	541218	560601	MONTGOMERY/GUNTER AFB	AL US	13821 13895
BLV	13802	72433	38.33	89.59	136	507705	520331	BELLEVILLE/SCOTT AFB	IL US	
BLV	13802	72433	38.33	89.59	133	523401	550911	BELLEVILLE/SCOTT AFB	IL US	
BLV	13802	72433	38.33	89.31	133	595228	590930	BELLEVILLE/SCOTT AFB	IL US	
BAK	13803	72436	39.16	85.54	199?	553515	550911	COLUMBUS/BAKALAR AFB	IN US	
FTK	13807	72423	37.54	85.58	230	540516	541002	FT KNOX/GODMAN AFB	KY US	
BYH	13814	72340	35.58	89.57	77	570301	580531	BLYTHEVILLE AFB	AR US	93821
BYH	13814	72340	35.58	89.57	80	603215	600522	BLYTHEVILLE AFB	AR US	
BYH	13814	72340	35.58	89.57	82	610299	640799	BLYTHEVILLE AFB	AR US	
NAB	13815	72216	31.35	84.06	61	560215	560531	ALBANY/TURNER AFB	GA US	
NAB	13815	72216	31.35	84.06	66	590215	590531	ALBANY/TURNER AFB	GA US	
NAB	13815	72216	31.35	84.07	65	600201	600517	ALBANY/TURNER AFB	GA US	
MXF	13821	72226	32.24	86.21	50	463301	500131	MONTGOMERY/MAXWELL	AL US	13895 13801
MXF	13821	72226	32.24	86.21	52	500201	541217	MONTGOMERY/MAXWELL	AL US	14849
DAY	13840	72429	39.52	84.07	297	511201	560430	DAYTON/WRIGHT PATTERSON	OH US	
DAY	13840	72429	39.52	84.07	297	560501	691114	DAYTON/SULPHUR GROVE (WB)	OH US	
DAY	13840	72429	39.52	84.07	299	691115	710708	DAYTON/SULPHUR GROVE	OH US	
DAY	13840	72429	39.52	84.07	298	710709		DAYTON/SULPHUR GROVE	OH US	
IIN	13841	72721	39.26	83.48	323	461001	491037	WILMINGTON/CLINTON AFB	OH US	
VFS	13858	72221	30.31	86.35	28	451201	511021	VALPARAISO/ELGIN AFB	FL US	
VFS	13858	72221	30.31	86.35	18	511021	540314	VALPARAISO/ELGIN AFB	FL US	
VFS	13858	72221	30.31	86.35	20	540315		VALPARAISO/ELGIN AFB	FL US	
WRB	13860	72217	32.38	83.38	86	481115	490125	WARNER ROBINS	GA US	
WRB	13860	72217	32.36	83.34	90	490125	540228	WARNER ROBINS	GA US	
WRB	13860	72217	32.36	83.34	86	540301	540430	WARNER ROBINS	GA US	
AYS	13861	72213	31.15	82.24	44	690415		WAYCROSS	GA US	13889
MEM	13862	72334	35.03	89.59	78	530301	530514	MEMPHIS	TN US	
MEM	13862	72334	35.03	89.59	83	540201	550430	MEMPHIS	TN US	
MEM	13862	72334	35.09	90.03	80	560215	560630	MEMPHIS	TN US	
MEM	13862	72334	35.03	89.58	88	590215	590523	MEMPHIS	TN US	
AFN	13873	72311	33.57	83.19	246	550904		ATHENS	GA US	13874
ATL	13874	72219	33.39	84.25	309	390706	550903	ATLANTA	GA US	13873
CES	13880	72208	32.54	80.02	18	390714	500715	CHARLESTON	SC US	
CES	13880	72208	32.54	80.02	15	500716		CHARLESTON	SC US	
JAX	13889	72206	30.25	81.39	6	551101	600215	JACKSONVILLE	FL US	93837
JAX	13889	72206	30.25	81.39	5	600216	690414	JACKSONVILLE	FL US	13861
MGM	13895	72226	32.24	86.14	50	340703	380630	MONTGOMERY MAXWELL FLD	AL US	13821
MGM	13895	72226	32.24	86.24	61	560601	690520	MONTGOMERY DONNELLY FLD	AL US	13801
MGM	13895	72226	32.18	86.24	57	690521	741111	MONTGOMERY DONNELLY FLD	AL US	3881
BNA	13897	72327	36.07	86.41	180	380713	491231	NASHVILLE/BERRY FLD	TN US	
BNA	13897	72327	36.07	86.41	178	500101	630918	NASHVILLE/BERRY FLD	TN US	
BNA	13897	72327	36.15	86.34	181	630919	631027	NASHVILLE	TN US	
BNA	13897	72327	36.15	86.34	180	631028		NASHVILLE	TN US	
SEP	13901	72260	32.13	98.11	399	731103		STEPHENVILLE	TX US	13911
LTS	13902	72352	34.39	99.16	414	540201	580530	ALTUS AFB	OK US	
LTS	13902	72352	34.39	99.16	420	610201	610531	ALTUS AFB	OK US	
ADM	13903	72350	34.18	97.01	222	610317	610531	ARDMORE/GENE AJTRY AFB	TX US	
ADM	13903	72350	34.18	97.01	222	610317	610531	ARDMORE/GENE AJTRY AFB	TX US	
ADM	13905	72244	30.40	96.33	81	540201	560630	BRYAN AFB	TX US	
ADM	13905	72244	30.40	96.33	84	570205	580518	BRYAN AFB	TX US	
END	13909	72353	36.20	97.40	396	441101	520709	ENID/VANCE AFB	OK US	
DYS	13910	72266	32.26	99.51	545	570301	570531	ABILENE/DYESS AFB	TX US	
DYS	13910	72266	32.26	99.51	539	580301	580531	ABILENE/DYESS AFB	TX US	
DYS	13910	72266	32.26	99.51	547	590215	590531	ABILENE/DYESS AFB	TX US	
DYS	13910	72266	32.26	99.51	550	600215	610604	ABILENE/DYESS AFB	TX US	13962
FWH	13911	72259	32.46	97.27	194	480823	490720	FT WORTH/CARSWELL AFB	TX US	
FWH	13911	72259	32.46	97.27	178	450721	570303	FT WORTH/CARSWELL AFB	TX US	
FWH	13911	72259	32.46	97.27	180	570304	731029	FT WORTH/CARSWELL AFB	TX US	13901
T.K	13919	72354	35.26	97.23	383	480915	490918	OKLAHOMA CITY/TINKER AFB	OK US	
T.K	13919	72354	35.26	97.23	376	480919	510114	OKLAHOMA CITY/TINKER AFB	OK US	
T.K	13919	72354	35.26	97.23	380	510115	520214	OKLAHOMA CITY/TINKER AFB	OK US	
T.K	13919	72354	35.26	97.23	375	520215	531229	OKLAHOMA CITY/TINKER AFB	OK US	
T.K	13919	72354	35.26	97.23	390	531230	590825	OKLAHOMA CITY/TINKER AFB	OK US	
T.K	13919	72354	35.26	97.23	387	590826	670630	OKLAHOMA CITY/TINKER AFB	OK US	

(380701-450123 MISG)
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af to wb 560501

some obs simul w/okc

APPENDIX B(2) (Continued)

Station History for North American Upper-air Stations

TIK 13919	72354	35.25?	97.23?	386?	670701	731231	OKLAHOMA CITY/TINKER AFB	OK US	13967	3948	archive mis 710331-731231
FOE 13920	72456	38.57	95.40	329	531221	540201	TOPEKA/FORBES AFB	KS US	13921		
FOE 13921	72456	38.57	95.40	321	540202	550929	TOPEKA/FORBES AFB	KS US		13996	
FLV 13922	72457	39.20	94.55	267	440599	480826	FT LEAVENWORTH/SHERMAN A	KS US			
FLV 13921	72457	39.19	94.55	274	480827	510531	FT LEAVENWORTH/SHERMAN A	KS US			
FLV 13921	72457	39.19	94.55	327	510601	531019	FT LEAVENWORTH/SHERMAN A	KS US		13920	
SLM 13922	72458	38.48	97.38	383	440799	550999	SALINA/SMOKY HILL AFB	KS US			
SLM 13922	72458	38.48	97.38	386	560214	560999	SALINA/SMOKY HILL AFB	KS US			
SLM 13922	72458	38.48	97.38	385	570301	581015	SALINA/SMOKY HILL AFB	KS US			
HKS 13927	72235	32.20	90.14	105	530301	530531	JACKSON/HAWKINS FLD	MS US			
HKS 13927	72235	32.20	90.13	98	540126	540430	JACKSON/HAWKINS FLD	MS US			
HKS 13927	72235	32.20	90.13	96	550215	550430	JACKSON/HAWKINS FLD	MS US		13939	
HKS 13927	72235	32.20	90.13	96	550215	550430	JACKSON/HAWKINS FLD	MS US		13956	
?	13928	72256	31.38	97.04	145	450199	450599	WACO/JAMES CONNALLY AFB	TX US		
?	13928	72256	31.38	97.16	145	510117	510416	WACO/JAMES CONNALLY AFB	TX US		
?	13928	72256	31.38	97.04	138	520229	520615	WACO/JAMES CONNALLY AFB	TX US		
?	13928	72256	31.38	98.30	326	500316	500531?	WICHITA FALLS/SHEPPARD	TX US		
SPS 13931	72351	33.59	98.30	326	500316	500531?	WICHITA FALLS/SHEPPARD	TX US			
AEX 13934	72246	31.19	92.33	27	550215	550430?	ALEXANDRIA	LA US			
GLE 13939	72238	33.28	90.59	41	540226	540430	GREENVILLE	MS US		13927	
LCH 13941	72240	30.13	93.09	5	410724	611231	LAKE CHARLES	LA US		3937	
BAD 13944	72248	32.30	93.41	49	480824	520211	SHREVEPORT/BARKSDALE AFB	LA US			
BAD 13944	72248	32.30	93.41	53	520212	560110	SHREVEPORT/BARKSDALE AFB	LA US		13957	
BAD 13944	72248	32.30	93.41	53	520212	560110	SHREVEPORT/BARKSDALE AFB	LA US			
FBI 13945	72355	34.39	98.24	365	600215	600330	LAWTON	OK US			
FBI 13947	72455	39.03	96.46	324	580404	581012	FT RILEY/MARSHALL AAF	KS US		13927	
FBI 13947	72455	39.03	96.46	324	690799		FT RILEY/MARSHALL AAF	KS US			
HKS 13956	72235	32.20	90.13	101	560201	600219	JACKSON/HAWKINS FLD	MS US		3940	
HKS 13956	72235	32.20	90.13	94	60220	681015	JACKSON/HAWKINS FLD	MS US		13944	
SHV 13957	72248	32.28	93.49	77	560111	560426	SHREVEPORT MUN AP	LA US			
SHV 13957	72248	32.28	93.49	76	560427	600319	SHREVEPORT MUN AP	LA US			
SHV 13957	72248	32.28	93.49	79	600320	750707	SHREVEPORT MUN AP	LA US		3951	
ACT 13959	72256	31.37	97.13	157	530599	530599	WACO	TX US		13928 W	
ABI 13962	72266	32.26	99.41	534	630204	730526	ABILENE	TX US		13910	
LIT 13963	72340	34.44	92.14	79	431010	550128	LITTLE ROCK	AR US			
LIT 13963	72340	34.44	92.14	87	550129	561222	LITTLE ROCK	AR US			
LIT 13963	72340	34.44	92.14	79	561223	751219	LITTLE ROCK	AR US		3952	
OKC 13967	72353	35.24	97.36	391	380717	550799	OKLAHOMA CITY/WILL ROGER	OK US			
OKC 13967	72353	35.24	97.36	392	550799	670630	OKLAHOMA CITY/WILL ROGER	OK US		13919	
OKC 13967	72353	35.24	97.36	392	750107	890327	OKLAHOMA CITY/WILL ROGER	OK US		3948	
COU 13983	72445	38.58	92.22	239	460202	510199	COLUMBIA	MO US		13994	
COU 13983	72445	38.58	92.22	238	510116	700827	COLUMBIA	MO US		3946	
DDC 13985	72451	37.46	99.58	800	430828	551225	DODGE CITY	KS US			
DDC 13985	72451	37.46	99.58	792	551226	631227	DODGE CITY	KS US			
DDC 13985	72451	37.46	99.58	791	631228		DODGE CITY	KS US		13983	
STL 13994	72434	38.45	90.23	181	390901	460129	ST LOUIS	MO US			
TOF 13996	72456	39.04	95.37	269	550930	681231	TOPEKA	KS US		13920	
TOF 13996	72456	39.04	95.37	268	690101		TOPEKA	KS US			
YQX 14501	72803	48.57	54.34	147	431208	450831	GANDER	NF CN		14509 W	
YJ7 14503	72815	48.33	58.34	5	440599	530107	STEPHENSVILLE/HARMON AFB	NF CN			
YJ7 14503	72815	48.33	58.34	59	530108	580727	STEPHENSVILLE/HARMON AFB	NF CN			
YJ7 14503	72815	48.33	58.34	30	580728	661210	STEPHENSVILLE/HARMON AFB	NF CN			
YJ7 14503	72815	48.33	58.34	60	661211	690899	STEPHENSVILLE/HARMON AFB	NF CN			
YJ7 14503	72815	48.32	58.33	60	690916	770630	STEPHENSVILLE/HARMON AFB	NF CN			
YJ7 14503	71815	48.32	58.33	60	770701	901231	STEPHENSVILLE/HARMON AFB	NF CN		14539	
YJ7 14503	71815	48.32	58.33	60	770701	901231	STEPHENSVILLE/HARMON AFB	NF CN		14508	
YAE 14508	72807	47.18	53.59	17	410501	500607	ARGENTIA	NF CN		14505	
YAE 14508	72807	47.18	53.59	17	520801	590731	ARGENTIA	NF CN		14505	
YAE 14508	72807	47.18	53.59	19	590801	700430	ARGENTIA	NF CN		14531	
YQX 14509	72803	48.57	54.34	140	410699	440899	GANDER	NF CN		14510	
YQX 14510	72803	48.09	55.21	3	440899	460699	BOTWOOD	NF CN		14509	
YJ7 14531	72801	47.40	52.45	140	710427	770630	TORBAI/ST JOHNS	NF CN		14508	
YJ7 14531	71801	47.40	52.45	140	770701		TORBAI/ST JOHNS	NF CN			
YJ7 14539	71815	48.32	58.33	60	910101		STEPHENSVILLE	NF CN			
PQ1 14604	72713	46.41	68.03	148	450401	460211	PRESQUE ISLE	ME US			
CAF 14607	72712	46.52	68.01	192	420403	481130	CARIBOU	ME US		14607 W	
CAF 14607	72712	46.52	68.01	194	48.201	501031	CARIBOU	ME US			
CAF 14607	72712	46.52	68.01	191	50.101	530525	CARIBOU	ME US			

Station History for North American Upper-air Stations

CAR	14607	72712	46.52	68.01	197	530526	540303	CARIBOU	ME US
CAR	14607	72712	46.52	68.01	191	540904		CARIBOU	ME US
NZ	14611	74392	43.53	69.56	36	530303	550519	BRUNSWICK	ME US
YSA	14642	72600	43.56	60.01	3	440899	570799	SABLE ISLAND	NS CN
YSA	14642	72600	43.56	60.02	3	570801	620930	SABLE ISLAND	NS CN
YSA	14642	72600	43.56	60.01	4	621001	770530	SABLE ISLAND	NS CN
YSA	14642	71600	43.56	60.01	4	770701		SABLE ISLAND	NS CN
CHH	14684	74494	41.40	69.58	16	771118		CHATHAM	MA US
YCX	14685	72701	45.51?	66.27?	36?	710104	720199	GAGETOWN	NB CN
YCX	14685	72701	45.50	66.26	52	720501	770530	GAGETOWN	NB CN
YCX	14685	71701	45.50	66.26	52	770701		GAGETOWN	NB CN
WOS	14688	74399	43.43	65.15	30	721101	761231	SHELBOURNE	NS CN
WOS	14693	74399	43.43	65.15	30	770101	770530	SHELBOURNE	NS CN
WOS	14693	71399	43.43	65.15	30	770701	880831	SHELBOURNE	NS CN
AGC	14701	72520	40.21	79.56	388	440829	450228	PITTSBURGH/ALLEGHENY APT	PA US
FNH	14704	72506	41.39	70.31	41	640714	650801	FALMOUTH	MA US
NY9?	14708	74498	40.44	73.36	23	520309	560318	NEW YORK/HEMPSTEAD	NY US
SWF	14714	74482	41.30	74.06	141	470516	500317	NEWBURGH/STEWART AFB	NY US
RME	14717	72518	43.14	75.25	146	470520	530312	NEWBURGH/STEWART AFB	NY US
RME	14717	72518	43.14	75.25	152	530313	551011	ROME/GRIFFISS AFB	NY US
PHM	14724	72606	43.39	70.15	23	440104	450702	PORTLAND/FT WILLIAMS	ME US
BUF	14733	72528	42.56	78.44	220	390901	540314	BUFFALO/GRTR ARPT	NY US
BUF	14733	72528	42.56	78.44	218	630820		BUFFALO/GRTR ARPT	NY US
ALB	14735	72518	42.45	73.48	94	430424	511130	ALBANY	NY US
ALB	14735	72518	42.45	73.48	86	551019		ALBANY	NY US
ACK	14756	72506	41.15	70.04	14	460416	501121	NANTUCKET	MA US
ACK	14756	72506	41.15	70.04	20	521122	510228	NANTUCKET	MA US
ACK	14756	72506	41.15	70.04	14	510301	691114	NANTUCKET	MA US
ACK	14756	72506	41.15	70.04	13	691115	701103	NANTUCKET	MA US
ACK	14756	72506	41.15	70.04	13	691115	701103	NANTUCKET	MA US
PHM	14762	72520	40.21	79.56	382	430430	520314	PITTSBURGH/ALLEGHENY	PA US
PHM	14764	72606	43.39	70.19	23	390701	550507	PORTLAND	ME US
PHM	14764	72606	43.39	70.19	20	550608		PORTLAND	ME US
?14779	99999	40.18	74.03	16	471201	480229	RED BANK	NJ US	
NEL	14780	72409	40.02	74.19?	39	391001	441199	LAKEHURST	NJ US
NEL	14780	72409	40.02	74.19	40	450399	550715	LAKEHURST/NAS	NJ US
NCO	14788	72507	41.35	71.25	10	431299	540799?	QUONSET POINT	RI US
MTC	14804	72537	42.37	82.50	176	451201	520229	MT CLEMENS	MI US
MTC	14804	72537	42.36	82.51	178	520301	560318	MT CLEMENS	MI US
RAN	14806	72531	40.18	88.09	227	440902	560911	PANTOUL/CRANU'VE AFB	IL US
?14809	72520	40.32	80.14	353	450301	540126	PITTSBURGH/CORAOPOLIS	PA US	
FNT	14826	72637	42.58	83.44	234	560919	681231	FLINT/BISHOP ARPT	MI US
FNT	14826	72637	42.58	83.44	236	690101		FLINT/BISHOP ARPT	MI US
JOT	14834	72534	41.30	88.10	179	390701	530314	JOLIET	IL US
PIA	14842	72532	40.40	89.41	201	560912	590330	PEORIA	IL US
PIA	14842	72532	40.40	89.41	200	591001		PEORIA	IL US
SSM	14847	72734	46.28	84.22	225	330718	531204	SAULT STE MARIE	MI US
SSM	14847	72734	46.28	84.22	221	531205	910518	SAULT STE MARIE	MI US
Y62	14847	72734	46.28	84.22	221	910619		SAULT STE MARIE	MI US
TOL	14849	72536	41.34	83.28	191	440104	511130	TOLEDO	OH US
YIP	14853	72537?	42.14	83.32	218	420715	431230	DETROIT/WILLOW RUN	MI US
GRB	14898	72645	44.29	88.08	210	450403	631122	GREEN BAY	WI US
GRB	14898	72645	44.29	88.08	209	631123	640813	GREEN BAY	WI US
GRB	14898	72645	44.29	88.08	210	640814		GREEN BAY	WI US
INL	14918	72747	48.36	93.14	343	420928	460719	INTERNATIONAL FALLS	MN US
INL	14918	72747	48.34	93.23	360	460720	521130	INTERNATIONAL FALLS	MN US
INL	14918	72747	48.34	93.23	368	521201	541130	INTERNATIONAL FALLS	MN US
INL	14918	72747	48.34	93.23	360	541201	691031	INTERNATIONAL FALLS	MN US
INL	14918	72747	48.34	93.23	359	691101		INTERNATIONAL FALLS	MN US
SFC	14926	72655	45.35	94.11	317	470524	511099	ST CLOUD/WHITNEY APT	MN US
SFC	14926	72655	45.35	94.11	316	511099	720209	ST CLOUD/WHITNEY APT	MN US
SFC	14926	72655	45.35	94.05	315	720215		ST CLOUD/MUNICIPAL APT	MN US
STP	14927	72657	44.56	93.04	224	411231	470520	ST PAUL	MN US
HON	14936	72654	44.23	98.13	391	630606	630817	HURON	SD US
HON	14936	72654	44.23	98.13	393	630818	690501	HURON	SD US
HON	14936	72654	44.23	98.13	392	690602		HURON	SD US

AES LON CHANGE 610999?
AES LON CHANGE 610999?

14756

14693

14688

94620 14762 W

14809 14762 W

94789

14735 SOME OBS SIMUL W/14735

14735 14764 W

4738

4738

14717 SOME OBS SIMUL W/14717

14717

14684

94823

LON MAY HAVE CHANGED
5204 CLOSING?...W#54742?

14826

14842

14701 14762 W SEE ALSO 94823

14804

14806

CALL LETTER CHANGE

CURRENT WMO#

14853 13840

94847 14849

14927

14926

94913

JUN-SEP 63-73 ONLY

Station History for North American Upper-air Stations

Station	17602	17605	GL	17601	17602	17605
GTL 17602	4202	76.33	68.49	520731	W. THULE	GL
GTL 17605	4202	76.33	68.49	601031	W THULE	GL
YAB 17801	72918	73.00	85.17	440899	ARCTIC BAY	NW CN
YAB 17801	71917	79.59	85.56	10	EUREKA	NW CN
YAB 17802	72918	73.00	85.18	11	ARCTIC BAY	NW CN
YRB 17901	72924	74.41	94.55?	471024	RESOLUTE	NW CN
YRB 17901	72924	74.41	94.54	62	RESOLUTE	NW CN
YRB 17901	72924	74.41	94.55	17	RESOLUTE	NW CN
YRB 17901	72924	74.41	94.54	62	RESOLUTE	NW CN
YRB 17901	72924	74.43	94.59	62	RESOLUTE	NW CN
YRB 17901	72924	74.43	94.59	64	RESOLUTE	NW CN
YRB 17901	72924	74.43	94.59	40	RESOLUTE	NW CN
YRB 17901	71924	74.43	94.59	40	RESOLUTE	NW CN
YRB 17906	71924	74.42	94.59	40	RESOLUTE	NW CN
YLT 18601	74082	82.32	62.42	66	ALERT	NW CN
YLT 18601	74082	82.30	62.20	66	ALERT	NW CN
YLT 18601	71082	82.30	62.20	66	ALERT	NW CN
YLT 18605	71082	82.30	62.20	66	ALERT	NW CN
YEU 18801	72917	80.13	86.11	4	EUREKA	NW CN
YEU 18801	72917	79.59?	85.56?	4	EUREKA	NW CN
YEU 18801	72917	79.59	85.57	4	EUREKA	NW CN
YEU 18801	72917	80.00	85.56	4	EUREKA	NW CN
YEU 18801	72917	80.06	85.57	7	EUREKA	NW CN
YEU 18801	72917	80.06	85.57	10	EUREKA	NW CN
YEU 18801	72917	79.59	85.56	10	EUREKA	NW CN
YEU 18801	71917	79.59	85.56	10	EUREKA	NW CN
YEU 18801	71917	79.59	85.56	3	MANZANILLO	MX
SIC 21101	76723	18.14	111.03	35	SOCORRO ISLAND	MX
SIC 21101	76723	18.43	110.57	34	SOCORRO ISLAND	MX
ITO 21504	91235	19.44	155.04	9	HILO	HI US
ITO 21504	91235	19.44	155.04	11	HILO	HI US
ITO 21504	91235	19.43	155.04	11	HILO	HI US
ITO 21504	91235	19.43	155.04	10	HILO	HI US
DLF 22001	72261	29.22	100.53	333	DEL RIO/LAUGHLIN AFB	TX US
DLF 22001	72261	29.22	100.47	333	DEL RIO/LAUGHLIN AFB	TX US
DLF 22001	72261	29.22	100.46	333	DEL RIO/LAUGHLIN AFB	TX US
DLF 22001	72261	29.22	100.46	333	DEL RIO/LAUGHLIN AFB	TX US
MCV 22007	76225	28.38	106.04	1428	CHIHUAHUA	MX
MCV 22007	76225	28.42	106.04	1428	CHIHUAHUA	MX
MZT 22009	76180	23.11	106.25	14	MAZATLAN SINALOA	MX
MZT 22009	76458	23.11	106.25	14	MAZATLAN SINALOA	MX
MZT 22009	76458	23.11	106.25	4	MAZATLAN SINALOA	MX
DRT 22010	72261	29.22	100.55	313	DEL RIO	TX US
MTY 22012	76394	25.52	100.15	423	MONTERREY	MX
MTY 22012	76394	25.52	100.12	450	MONTERREY	MX
MTY 22013	76612	20.41	103.20	1551	GUADALAJARA	MX
MTY 22104	76256	27.57	110.48	12	EMPALME SONORA	MX
GYM 22104	76256	27.57	110.48	12	EMPALME SONORA	MX
GYP 22105	76151	28.52	118.15	23	GUADALUPE ISLAND	MX
YEV 22258	72957	68.19	133.32	103	INUVIK (UA)	NW CN
YEV 22258	71957	68.19	133.32	103	INUVIK (UA)	NW CN
BKH 22501	91182	22.02	159.47	5	BARKING SANDS	HI US
BKH 22504	91182	21.20	157.57	8	HONOLULU/ (HICKAM FLD)	HI US
NPS 22517	91199	21.21	157.57	7	PEARL HARBOR	HI US
NPS 22517	91199	21.21	157.57	3	PEARL HARBOR	HI US
HNL 22521	91182	21.20	157.55	4	HONOLULU/JOHN ROGERS FLD	HI US
HNL 22521	91182	21.20	157.55	3	HONOLULU/JOHN ROGERS FLD	HI US
HNL 22521	91182	21.20	157.55	4	HONOLULU INT AP	HI US
HNL 22521	91182	21.20	157.55	4	HONOLULU INT AP	HI US
LTH 22536	91165	21.58	159.22	36	LIHUE/KAUAI	HI US
LTH 22536	91165	21.59	159.21	36	LIHUE/KAUAI	HI US
BKH 22545	91162	22.02	159.47	8	BARKING SANDS	HI US
BKH 22545	91162	22.02	159.47	5	BARKING SANDS	HI US
FFS 22604	91115	23.52	166.17	6	FRENCH FRIGATE SHOAL	HI US
MDY 22701	91066	28.13	177.22	13	MIDWAY ISLAND (NAVY)	PC US
MDY 22701	91066	28.13	177.22	13	MIDWAY ISLAND (NAVY)	PC US
MDY 22701	91066	28.13	177.22	13	MIDWAY ISLAND (NAVY)	PC US
MDY 22701	91066	28.13	177.22	13	MIDWAY ISLAND (NAVY)	PC US
MDY 22701	91066	28.13	177.21	8	MIDWAY ISLAND (NAVY)	PC US

DESCREPAANCIES IN HISTORY

CANADIAN CONTROL 610101
WBAN NUMBER CHANGE
WBAN NUMBER CHANGE

WBAN NUMBER CHANGE
WBAN NUMBER CHANGE

("CN CONTROL" 610101)
WBAN NUMBER CHANGE
WBAN NUMBER CHANGE

CALL LETTERS "CJU" ASO

Station History for North American Upper-air Stations

MDY 22701	91066	28.13	177.21	12	561230	570124	MIDWAY ISLAND (NAVY)	PC US	
MDY 22702	91066	28.13	177.21	3	57C125		MIDWAY ISLAND (NAVY)	PC US	
MDY 22703	91066	28.13	177.22	13	461007	480430	MIDWAY ISLAND (ARMY)	PC US	22701 22701
BMN 23002	74732	32.51	106.05	1247	506606	520527	MIDWAY ISLAND (WB)	PC US	22701 22701 23039
AMA 23003	72363	35.13	101.50	1099	48C301		ALAMOGORDO/HOLLOMAN AFB	NM US	
AMA 23003	72363	35.13	101.50	1096	52C215	521068	AMARILLO	TX US	
AMA 23003	72363	35.13	101.50	1099	521009	561068	AMARILLO	TX US	
AMA 23003	72363	35.14	101.42	1096	561125	561261	AMARILLO	TX US	23047
LYR 23012	72469	39.43	104.53	1640	481015	490220	DENVER/LOWRY	CO US	
LYR 23012	72469	39.43	104.53	1643	49C221	500107	DENVER/LOWRY	CO US	
LYR 23012	72469	39.43	104.53	1640	50C108	521212	DENVER/LOWRY	CO US	
LYR 23012	72469	39.43	104.52	1661	521213	560814	DENVER/LOWRY	CO US	23062
GOF 23017	72265	31.24	100.24	569	53C399	690959	SAN ANGELO/GOODFELLOW	TX US	
GOF 23017	72265	31.24	100.24	573	70C201	710131	SAN ANGELO/GOODFELLOW	TX US	
ELP 23019	72270	31.50	106.24	1207	44C617	460522	EL PASO/BIGGS AFB	?TX US	23044 W
REE 23021	72267	33.35	102.14	1015	50C301	500613	LUBBOCK/REESE AFB	TX US	
REE 23021	72267	33.36	102.15	1014	52C215	520625	LUBBOCK/REESE AFB	TX US	
REE 23021	72267	33.36	102.02	1017	60C315	640518	LUBBOCK/REESE AFB	TX US	
MRF 23022	72264	30.22	104.01	1478	59C215	590520	MARFA AAF	TX US	
MAF 23023	72265	31.56	102.12	871	531115	591231	MIDLAND	TX US	
MAF 23023	72265	31.56	102.12	880	60C101	600419	MIDLAND	TX US	23041
MAF 23023	72265	31.56	102.12	874	60C420	720229	MIDLAND	TX US	
MAF 23023	72265	31.56	102.12	873	72C301	720412	MIDLAND	TX US	
MAF 23023	72265	31.56	102.12	870	72C413	720417	MIDLAND	TX US	
GJT 23032	72476	39.04	108.34	1404	44C501	440959	GRAND JUNCTION	CO US	23066
23037	99999?	32.24	106.09	1260	46C523	480430	OROGRADE	NM US	
23038	99999?	31.47	106.25	1184	48C323	481204	FT. BLISS	TX US	
23039	72269	32.22	106.28	1381	461107	470515	WHITE SANDS/LAS CRUCES	NM US	23002
23039	72269	32.24	106.24	1211	47C516	471021	WHITE SANDS/LAS CRUCES	NM US	
23039	72269	32.24	106.21	1216	471023		WHITE SANDS/LAS CRUCES	NM US	
23041	72265	32.14	101.30	774	431010	501231	BIG SFR USING	TX US	
23041	72265	32.14	101.30	784	51C101	531113	BIG SFR USING	TX US	23023
ELP 23044	72270	31.49	106.24	1195	39C712	570630	EL PASO	TX US	
ELP 23044	72270	31.49	106.24	1197	57C701	600731	EL PASO	TX US	
ELP 23044	72270	31.48	106.24	1193	60C801	831202	EL PASO	TX US	
ELP 23044	72270	31.48	106.24	1199	831203		EL PASO	TX US	
AMA 23047	72363	35.14	101.42	1098	561201	561230	AMARILLO	TX US	23003
AMA 23047	72363	35.14	101.42	1095	561231		AMARILLO	TX US	
ABC 23050	72365	35.03	106.37	1620	39C318	510904	ALBUQUERQUE	NM US	
ABC 23050	72365	35.03	106.37	1619	51C905		ALBUQUERQUE	NM US	
DEN 23062	72469	39.46	104.53	1608	56C815	561113	DENVER/STAPLETON ARPT	CO US	23012
DEN 23062	72469	39.46	104.53	1611	561114		DENVER/STAPLETON ARPT	CO US	
GLD 23065	72465	39.21	101.42	1124	59C699	590959	GOODLAND	KS US	
GJT 23066	72476	39.07	108.32	1474	441130	530810	GRAND JUNCTION	CO US	
GJT 23066	72476	39.07	108.32	1481	53C811	561101	GRAND JUNCTION	CO US	23032
GJT 23066	72476	39.07	108.32	1474	561102	681231	GRAND JUNCTION	CO US	
GJT 23066	72476	39.07	108.32	1472	69C101		GRAND JUNCTION	CO US	
FAT 23106	72389	36.46	119.42	103	45C799	451259	FRESNO	CA US	
FAT 23106	72389	36.49	119.42	103	52C208	550469	FRESNO	CA US	
DMA 23109	72274	32.10	110.54	811	45C721	560301	TUSCON/DAVIS MONTHAN AFB	AZ US	23160
LSV 23112	72386	36.15	115.02	572	45C799	460159	NELLIS AFB	NV US	23169 W
LSV 23112	72386	36.15	115.02	569	50C829	540201	NELLIS AFB	NV US	
EDW 23114	72381	34.54	117.54	725	50C301	560320	MURC/EDWARDS AFB	CA US	
EDW 23114	72381	34.55	117.54	725	56C321		MURC/EDWARDS AFB	CA US	
RAA 23118	72488	39.40	119.52	1555	531015	531212	RENO/STEAD AFB	NV US	
RAA 23118	72488	39.40	119.52	1530	55C201	550207	RENO/STEAD AFB	NV US	
RAA 23118	72488	39.40	119.52	1545	55C208	570923	RENO/STEAD AFB	NV US	
LAX 23124	72295	34.04	118.26	147	441099	450959	LOS ANGELES	CA US	23129
TPH 23128	72485	38.04	117.05	1652	511008	550515	TONOPAH	NV US	3132
LGB 23129	72297	33.49	118.09	20	47C310	511159	LONG BEACH	CA US	23124
LGB 23129	72297	33.49	118.09	22	511199	520459	LONG BEACH	CA US	
LGB 23129	72297	33.49	118.09	18	520499	530416	LONG BEACH	CA US	
LGB 23129	72297	33.50?	118.09	20	530417	551231	LONG BEACH	CA US	
LGB 23129	72297	33.50	118.09	18	56C101	560416	LONG BEACH	CA US	93197

Station History for North American Upper-air Stations

Station	Time	Altitude	Frequency	Station	Time	Altitude	Frequency	Station	Time	Altitude	Frequency
LAX	23145	72295	33.56	118.23	29	450399	451099	LOS ANGELES	CA US		
Ely	23154	72486	39.17	114.52	1908	390724	531028	Ely	NV US		
Ely	23154	72486	39.17	114.51	1908	540601		Ely	NV US		
TUS	23160	72274	32.08	110.57	781	560301	581020	TUCSON	AL US	23109	
TUS	23160	72274	32.07	110.56	789	581021	600420	TUCSON	AL US		
TUS	23160	72274	32.08	110.57	789	600421	601231	TUCSON	AL US		
TUS	23160	72274	32.07	110.56	789	610101	860327	TUCSON	AL US		
TUS	23160	72274	32.07	110.56	788	860328		TUCSON	AL US		
LAS	23169	72386	36.05	115.10	650	520801	661009	LAS VEGAS	NV US	23173	3133
LAS	23173	72386	36.05	115.10	650	450925	520731	LAS VEGAS	NV US		23169
LAX	23174	72295	33.56	118.23	39	650902	650916	LOS ANGELES	CA US		
LAX	23174	72295	33.56	118.23	32	650917	650924	LOS ANGELES	CA US		3197
LAX	23174	72295	33.56	118.23	32	650925	710430	LOS ANGELES	CA US		
LAX	23174	72295	33.56	118.24	32	650925	710430	LOS ANGELES	CA US		
PHX	23183	72278	33.26	112.02	388	390721	521130	PHOENIX	AL US		
PHX	23183	72278	33.26	112.02	341	521201	540431	PHOENIX	AL US		
PHX	23183	72278	33.26	112.01	341	540501	580115	PHOENIX	AL US		
PHX	23183	72278	33.26	112.02	341	541210	580115	PHOENIX	AL US		3149
INW	23194	72374	35.01	110.44	1492	611101	681231	WINSLOW	AL US		
INW	23194	72374	35.01	110.44	1487	690101		WINSLOW	AL US		
CIC	23201	72497	39.48	121.51	71	620206	710326	CHICO	CA US		
MER	23203	72481	37.22	120.34	57	440401	630131	MERCED/CASTLE AFB	CA US		
OAK	23230	72493	37.44	122.12	8	360901	501231	OAKLAND	CA US		
OAK	23230	72493	37.44	122.12	6	510101	661220	OAKLAND	CA US		
OAK	23230	72493	37.45	122.13	6	661221		OAKLAND INT AP	CA US		
SMX	23236	72394	34.56	120.25	71	430513	541021	SANTA MARIA	CA US	23273	
SMX	23273	72394	34.54	120.27	74	541022	590630	SANTA MARIA	CA US		23236
BFF	24007	72566	41.52	103.36	1204	530601	610925	SCOTTSDUFF	NE US		93215
BIS	24011	72764	46.46	100.45	505	390707	551031	BISMARCK	ND US		
BIS	24011	72764	46.46	100.45	511	551101	561130	BISMARCK	ND US		
BIS	24011	72764	46.46	100.45	505	561201	681231	BISMARCK	ND US		
BIS	24011	72764	46.46	100.45	503	690101		BISMARCK	ND US		
BIS	24021	72576	42.48	108.43	1698	450901	590831	LANDER	WY US		
LND	24021	72576	42.49	108.44	1696	590901	691031	LANDER	WY US		
LND	24021	72576	42.49	108.44	1697	691101	730919	LANDER	WY US		
LND	24021	72576	42.49	108.44	1695	730920		LANDER	WY US		
LBF	24023	72562	41.08	100.42	849	450106	520814	NORTH PLATTE	NE US		
LBF	24023	72562	41.08	100.41	848	520815	681231	NORTH PLATTE	NE US		
LBF	24023	72562	41.08	100.41	847	690101		NORTH PLATTE	NE US		
RAP	24026	72662	44.09	103.06	980	431006	501012	RAPID CITY	SD US	24090	
GCW	24034	72768	48.11	106.38	648	430606	551026	GLASGOW	MT US	94008	
RAP	24090	72662	44.09	103.06	966	501013	501031	RAPID CITY	SD US	24026	
RAP	24090	72662	44.02	103.02	966	501101	510930	RAPID CITY	SD US		
RAP	24090	72662	44.02	103.03	966	511001	610321	RAPID CITY	SD US		
RAP	24090	72662	44.03	103.04	966	610322		RAPID CITY	SD US		
HIF	24101	72575	41.07	112.01	1451	481105	500818	OGDEN/HILL AFB	UT US	24126	
HIF	24101	72575	41.07	112.01	1448	500819	511231	OGDEN/HILL AFB	UT US		
HIF	24101	72575	41.07	112.01	1450	520101	560807	OGDEN/HILL AFB	UT US	24127	
DFG	24103	72581	40.10	113.00	1325	491015	520215	TOOELE/DJGWAY PG	UT US	24111	
DFG	24103	72581	40.10	113.00	1329	520216	530430	TOOELE/DJGWAY PG	UT US		
DFG	24103	72581	40.11	112.55	1329	530501	570731	TOOELE/DJGWAY PG	UT US		
ENV	24111	72581	40.43	114.04	1292	470102	480909	WENDOVER AFB	UT US	24103	
GTF	24112	72775	47.31	111.10	1077	450599	531299	GREAT FALLS/MALMSTROM AF	MT US		24143 W
SLC	24127	72572	40.46	111.58	1288	430899	480831	OGDEN	UT US	24101	
WMC	24128	72583	40.54	117.48	1310	560501	680201	SALT LAKE CITY	UT US	24101	
WMC	24128	72583	40.54	117.48	1312	680202		WINNEMUCCA	NV US		
BOI	24131	72681	43.34	116.13	868	390901	670811	BOISE	ID US		
BOI	24131	72681	43.34	116.13	867	670811	690808	BOISE	ID US		
BOI	24131	72681	43.34	116.13	871	690809		BOISE	ID US		
GTF	24143	72775	47.30	111.21	1128	400801	530831	GREAT FALLS	MT US		
GTF	24143	72775	47.30	111.21	1123	530901	540430	GREAT FALLS	MT US		
GTF	24143	72775	47.29	111.21	1123	540501	681231	GREAT FALLS	MT US		
GEG	24157	72785	47.40	117.20	600	470126	471207	GREAT FALLS	MT US		
GEG	24157	72785	47.37	117.31	726	471208	510125	SPOKANE	WA US		
GEG	24157	72785	47.37	117.31	722	510126	651219	SPOKANE	WA US		

IRREGULAR OBS

dup dat w/94008 551001-26

Station History for North American Upper-air Stations

Station ID	Station Name	Lat	Long	Alt	Country	Remarks
GEG 21157	SPOKANE	47.37	117.31	651220	WA US	
GEG 21157	SPOKANE	47.37	117.31	690101	WA US	
GEG 21157	SPOKANE	47.38	117.32	690123	WA US	
GRF 21201	FT LEWIS/GRAY AFB	47.09	122.33	87 691001	WA US	24244 W
TCM 21201	TACOMA/MCHORD AFB	47.09	122.29	88 520404	WA US	24225 W
NEJ 21208	SEATTLE/BOEING FLD	47.32	122.18	40901	WA US	
MFR 21209	MEDFORD AFB	42.23	122.52	440901	OR US	24232
IAP 21211	PORTLAND	45.36	122.36	460101	OR US	
IAP 21211	PORTLAND	45.36	122.36	7 530202	OR US	
MFR 21225	MEDFORD	42.22	122.52	401 390901	OR US	
MFR 21225	MEDFORD	42.22	122.52	397 840814	OR US	
OLM 21227	OLYMPIA	46.58	122.54	58 620601	WA US	24233 24240
SLE 21232	SALEM	44.55	123.01	61 560601	WA US	24211 24244
SEA 21233	SEATTLE/TACOMA APT	47.27	122.18	124 560629	WA US	24227
SEA 21233	SEATTLE/TACOMA APT	47.27	122.18	125 560914	WA US	
TTI 21240	TATOOSH ISLAND	48.23	124.44	33 430315	WA US	24227 94240
TTI 21240	TATOOSH ISLAND	48.23	124.44	31 541015	WA US	
NEJ 21244	SEATTLE/NAS	47.41	122.16	10 450399	WA US	
NEJ 21244	SEATTLE/NAS	47.41	122.16	19 490499	WA US	24233
NEJ 21244	SEATTLE/NAS	47.41	122.16	10 540202	WA US	
YOD 25004	THE PAS	53.58	101.06	273 470499	MB CN	25051
YOD 25004	THE PAS	53.58	101.06	273 770701	SK CN	
YPA 25013	PRINCE ALBERT	53.13	105.41	428?	SK CN	
YOD 25051	THE PAS	53.58	101.06	274 910101	SK CN	25004
YXD 25102	EDMONTON	53.34	113.31	667 431259	AB CN	
YXD 25108	EDMONTON/NAMAQ AFB	53.40	113.29	697 440859	AB CN	
YXC 25110	CALGARY	51.06	114.01	10684?	AB CN	
YXC 25110	CALGARY	51.07	114.01	10684?	AB CN	
YXD 25111	EDMONTON/MUN AP	53.38	113.29	666 460259	AB CN	
YXD 25111	EDMONTON/MUN AP	53.34	113.31	668 531015	AB CN	25145
WSE 25145	EDMONTON/STONY PLAIN	53.33	114.06	166 660215	AB CN	
WSE 25145	EDMONTON/STONY PLAIN	53.33	114.06	166 770701	AB CN	25111
YVR 25152	VERNON	50.14	119.17	556?	BC CN	
YVR 25152	VERNON	50.14	119.17	556?	BC CN	
WIC 25154	PRIMROSE LAKE	54.48	110.05	703 670499	AB CN	
WIC 25154	PRIMROSE LAKE	54.48	110.05	703 770701	AB CN	
YRM 25159	ROCKY MTN HOUSE (UA)	52.26	114.54	988 690601	BC CN	
YXS 25206	PRINCE GEORGE	53.50	122.48	678?	BC CN	
YXS 25206	PRINCE GEORGE	53.54	122.40	676 441199	BC CN	
YXS 25206	PRINCE GEORGE	53.53	122.41	676 560199	BC CN	
YXS 25206	PRINCE GEORGE	53.53	122.40	676 720599	BC CN	
YXS 25206	PRINCE GEORGE	53.53	122.40	676 770701	BC CN	
YXS 25206	PRINCE GEORGE	53.53	122.41	675 860699	BC CN	
YXE 25218	FORT NELSON	58.50	122.35	375?	BC CN	
YXE 25218	FORT NELSON	58.50	122.35	373?	BC CN	
YXE 25218	FORT NELSON	58.50	122.35	379?	BC CN	
YXE 25218	FORT NELSON	58.50	122.35	379?	BC CN	
YZE 25223	PORT HARDY	50.41	127.22	23 460699	BC CN	25262
YZE 25223	PORT HARDY	50.41	127.22	19 500999	BC CN	
YZE 25223	PORT HARDY	50.41	127.22	17 640504	BC CN	
YZE 25223	PORT HARDY	50.41	127.22	17 770701	BC CN	
YZE 25262	FORT NELSON UA	58.50	122.36	377 830101	BC CN	
YZE 25273	PORT HARDY	50.41	127.22	17 910101	BC CN	
ANN 25301	ANNETTE ISLAND	55.02	131.34	35 440414	AK US	
YAK 25302	YAKUTAT	59.30	139.40	9 440417	AK US	
YAK 25302	YAKUTAT	59.30	139.41	35 460522	AK US	25339
ANN 25308	ANNETTE ISLAND	55.02	131.34	35 470710	AK US	25301
ANN 25308	ANNETTE ISLAND	55.02	131.34	37 510701	AK US	25325
JNU 25309	JUNEAU APT	58.22	134.33	6 390901	AK US	
JNU 25309	JUNEAU APT	58.22	134.35	6 430701	AK US	
KET 25325	KETCHIKAN	55.21	131.39	25 400920	AK US	25308
YAK 25339	YAKUTAT	59.31	139.40	10 480801	AK US	
YAK 25339	YAKUTAT	59.31	139.40	12 490601	AK US	
YAK 25339	YAKUTAT	59.31	139.40	10 491001	AK US	
ADQ 25501	YAKUTAT	57.44	152.31	34 420801	AK US	
ADQ 25501	KODIAK	57.45	152.30	20 450901	AK US	

NCDC HAS NO RECORD HERE
 W PPBB ONLY
 AES OPEN DATE 460199
 sim obs W 25145 880215-23
 sim obs W 25111 660215-23
 sim obs W 25111 660215-23
 NCDC ELE=555m
 (ROCKE)SONDE STW
 (ROCKE)SONDE STN
 AES CLOSE DATE 760799
 AES ELE=676m, OPEN=441199

AES OPEN DATE 420399

FROM COAL HARBOUR

WEAN # CHANGE
WEAN # CHANGE

CURRENT WMO# 70395

Station History for North American Upper-air Stations

ADQ 25501	70350	57.45	152.30	28	521210	530802	KODIAK	AK US	
ADQ 25501	70350	57.45	152.30	20	530803	570806	KODIAK	AK US	
ADQ 25501	70350	57.45	152.30	5	570807	600430	KODIAK	AK US	
ADQ 25501	70350	57.45	152.30	6	600501	630919	KODIAK	AK US	
ADQ 25501	70350	57.45	152.30	4	630920	730131	KODIAK	AK US	
ADQ 25501	70350	57.45	152.29	4	730201		KODIAK	AK US	
AKN 25503	70326	58.41	156.39	19	530505	540630	WAKNEK	AK US	
AKN 25503	70326	58.41	156.39	16	540701	551212	WAKNEK	AK US	
AKN 25503	70326	58.41	156.39	15	551213		WAKNEK	AK US	
?	25602	53.23	167.54	58	460614	470929	KING SALMON	AK US	RENAMED KING SALMON
?	25602	53.23	167.54	22	470930	501121	UMNAK/CAPE AFB/FT GLENN	AK US	
?	25602	53.23	167.54	33	451119	490812	COLD BAY AFB	AK US	25620
CDB 25603	70316	55.12	162.42	28	490813	500523	COLD BAY AFB	AK US	
CDB 25603	70316	55.12	162.42	25	500524	500930	COLD BAY AFB	AK US	
CDB 25603	70316	55.12	162.42	29	501001	521211	COLD BAY AFB	AK US	
CDB 25603	70316	55.12	162.42	24	530326	530831	COLD BAY AFB	AK US	
CDB 25603	70316	55.12	162.42	26	530901	540228	COLD BAY AFB	AK US	25624
ADU 25611	70489	53.54	166.32	7	520624	540724	DUTCH HARBOR	AK US	25602 25611
ADU 25620	70489	53.54	166.32	12	501211	520524	DUTCH HARBOR	AK US	25603
CDB 25624	70316	55.12	162.43	27	550820	610421	COLD BAY	AK US	
CDB 25624	70316	55.12	162.43	30	610422		COLD BAY	AK US	
ADK 25701	70454	51.53	176.31	4	440301	480624	ADAK/DAVIS AFB	AK US	25704
ADK 25701	70454	51.53	176.31	4	480625	500831	ADAK/DAVIS AFB	AK US	
ADK 25704	70454	51.53	176.39	38	421299	440299	ADAK	AK US	25701
ADK 25704	70454	51.53	176.39	20	500901	530615	ADAK/DAVIS AFB	AK US	
ADK 25704	70454	51.53	176.39	8	530616		ADAK/DAVIS AFB	AK US	
ADK 25705	70308	57.08	170.16	29	431199	450999	ST PAUL ISLAND	AK US	
ADK 25705	70308	57.08	170.16	29	451016	470623	ST PAUL ISLAND	AK US	
ADK 25713	70308	57.09	170.13	7	470701	480430	ST PAUL ISLAND	AK US	
ADK 25713	70308	57.09	170.13	9	480501	520131	ST PAUL ISLAND	AK US	
ADK 25713	70308	57.09	170.13	10	520201	560930	ST PAUL ISLAND	AK US	
ADK 25713	70308	57.09	170.13	15	561001	561130	ST PAUL ISLAND	AK US	
ADK 25713	70308	57.09	170.13	10	561201		ST PAUL ISLAND	AK US	
ADK 25713	70308	57.09	170.13	25	700217	770630	CAMBRIDGE BAY	AK US	26107 26010
ADK 25713	70308	57.09	170.13	25	770701	901231	CAMBRIDGE BAY	AK US	
ADK 25713	70308	57.09	170.13	25	910101		CAMBRIDGE BAY	AK US	26005
ADK 25713	70308	57.09	170.13	203	431299	441199?	FT SMITH	AK US	
ADK 25713	70308	57.09	170.13	203	460199	710930	FT SMITH	AK US	26118
ADK 25713	70308	57.09	170.13	203	471110	700217	COPPERMINE	AK US	26005
ADK 25713	70308	57.09	170.13	203	680201	770630	FT SMITH (UA)	AK US	26102
ADK 25713	70308	57.09	170.13	203	770701		FT SMITH (UA)	AK US	
ADK 25713	70308	57.09	170.13	203	770701		FT SMITH (UA)	AK US	
ADK 25713	70308	57.09	170.13	111	440399	441299	NORMAN WELLS	AK US	
ADK 25713	70308	57.09	170.13	75	450199	511114	NORMAN WELLS	AK US	
ADK 25713	70308	57.09	170.13	62	511115	670999	NORMAN WELLS	AK US	
ADK 25713	70308	57.09	170.13	63	671099	770630	NORMAN WELLS	AK US	
ADK 25713	70308	57.09	170.13	63	770701	841031	NORMAN WELLS	AK US	
ADK 25713	70308	57.09	170.13	95	841101		NORMAN WELLS (UA)	AK US	
ADK 25713	70308	57.09	170.13	633?	440699	460399	WHITEHORSE	AK US	
ADK 25713	70308	57.09	170.13	755?	460599	460999	WHITEHORSE	AK US	
ADK 25713	70308	57.09	170.13	698?	461099	620399	WHITEHORSE	AK US	
ADK 25713	70308	57.09	170.13	704	620499	770630	WHITEHORSE	AK US	
ADK 25713	70308	57.09	170.13	704	770701	901231	WHITEHORSE	AK US	26338
ADK 25713	70308	57.09	170.13	10	420999	600912	AKLAVIK	AK US	26323
ADK 25713	70308	57.09	170.13	58?	600912	730331	INUVIK	AK US	26316
ADK 25713	70308	57.09	170.13	704	910101		WHITEHORSE	AK US	26409
ADK 25713	70308	57.09	170.13	60	451011	460521	ANCHORAGE	AK US	
ADK 25713	70308	57.09	170.13	386	501111	510228	FORT GREENY	AK US	
ADK 25713	70308	57.09	170.13	392	510301	720314	FORT GREENY	AK US	26459
ADK 25713	70308	57.09	170.13	51	430202	451010	ANCHORAGE	AK US	26401
ADK 25713	70308	57.09	170.13	51	460522	520714	ANCHORAGE	AK US	
ADK 25713	70308	57.09	170.13	42	520715	531028	ANCHORAGE	AK US	
ADK 25713	70308	57.09	170.13	32	531029	541203	ANCHORAGE INT APT	AK US	
ADK 25713	70308	57.09	170.13	30	541204	590630	ANCHORAGE INT APT	AK US	
ADK 25713	70308	57.09	170.13	29	590701	640708	ANCHORAGE INT APT	AK US	
ADK 25713	70308	57.09	170.13	45	640709		ANCHORAGE IAP/PT.	AK US	
ADK 25713	70308	57.09	170.13	134	371009	510822	FAIRBANKS	AK US	

DESCREpancy ON WHEN OPEN
AES OPEN 441299-480599

AES OPEN DATE 480899

AES OPEN DATE 460599

WBAN NUMBER CHANGE
WBAN NUMBER CHANGE

AES ELE-68m WMO flm

Station History for North American Upper-air Stations

FBI 26411	70261	64.49	147.52	139	510823	520112	FAIRBANKS	AK US	
FBI 26411	70261	64.49	147.52	135	520113		FAIRBANKS	AK US	
CRF 26412	70291	62.58	141.58	524	421201	550512	NORTEWAY	AK US	
SFK 26459	70192	65.07	147.29	197	720602	999999?	POKER FLAT	AK US	26406
MCC 26510	70231	62.58	155.37	103	420411		MCCRATH	AK US	
OME 26604	70200	64.30	165.26	13	440417	460327	NOME AAB	AK US	
OME 26604	70200	64.30	165.28	14	460606	461009	NOME AAB	AK US	26617 26617
BET 26615	70219	60.47	161.41	8	401019	541031	BETHEL	AK US	
BET 26615	70219	60.47	161.43	4	541101	561106	BETHEL	AK US	
BET 26615	70219	60.47	161.43	11	561107	561231	BETHEL	AK US	
BET 26615	70219	60.47	161.48	4	570101	581110	BETHEL	AK US	
BET 26615	70219	60.47	161.48	39	581111	811101	BETHEL	AK US	
BET 26615	70219	60.47	161.48	36	811101		BETHEL	AK US	
OFZ 26616	70133	66.52	162.38	5	421026		KOTZEBUE	AK US	
OME 26617	70200	64.30	165.24	7	400915	421014	NOME FED BLDG	AK US	
OME 26617	70200	64.30	165.24	7	461020	481231	NOME FED BLDG	AK US	26604
OME 26617	70200	64.30	165.24	7	490101	501204	NOME AP	AK US	26604
OME 26617	70200	64.30	165.26	7	501205	520831	NOME AP	AK US	
OME 26617	70200	64.30	165.26	10	520901	660428	NOME AP	AK US	
OME 26617	70200	64.30	165.26	5	660429		NOME AP	AK US	
CTH 26636	70107	68.06	165.46	13	620325	620520	CAPE THOMPSON	AK US	12/1/-12/20/69 LOST
GAM 26703	70204	63.51	171.36	10	421111	530630	GAMBELL	AK US	
YIC 27001	74074	78.47	103.32	31	480818	590899	ISACENSEN	NW CN	
YIC 27001	74074	78.47	103.32	30	590699	770830	ISACENSEN	NW CN	
YIC 27001	74074	78.47	103.32	30	770701	780819	ISACENSEN	NW CN	
YMD 27101	74072	76.17	119.28	20	480601	601229	MOULD BAY	NW CN	
YMD 27101	74072	76.14	119.20	58	601230	770530	MOULD BAY	NW CN	
YMD 27101	71072	76.14	119.20	58	770701	901231	MOULD BAY	NW CN	27107
YMD 27101	71072	76.14	119.20	58	910101		MOULD BAY	NW CN	27101
YSY 27201	74051	71.57	124.44	84	551101	680630	SACHS HARBOUR	NW CN	
YSY 27201	74051	71.59	125.17	84	680701	770530	SACHS HARBOUR	NW CN	
YSY 27201	71051	71.59	125.17	84	770701	860715	SACHS HARBOUR	NW CN	
BFI 27401	70086	70.07	143.40	6	530327	561203	BARTER ISLAND AWS	AK US	
BFI 27401	70086	70.07	143.40	15	561210	571905	BARTER ISLAND	AK US	
BFI 27401	70086	70.08	143.43	15	571006	571106	BARTER ISLAND	AK US	
BFI 27401	70086	70.08	143.38	15	571107	890102	BARTER ISLAND	AK US	
BRW 27502	70026	71.18	156.47	10	400915	500531	POINT BARROW	AK US	
BRW 27502	70026	71.18	156.47	8	500601	770815	POINT BARROW	AK US	
BRW 27502	70026	71.18	156.47	12	770616		POINT BARROW	AK US	
AMC 45702	70439	51.24	179.16	46	440606	481104	AMCHITKA ISLAND	AK US	
AMC 45702	70439	51.23	179.15	68	481110	651030	AMCHITKA ISLAND	AK US	
SVA 45708	70414	52.43	174.04	20	450301	501231	SHEMYA ISLAND	AK US	
SVA 45708	70414	52.44	174.07	80	510101	540520	SHEMYA ISLAND AFB	AK US	45714
AFU 45709	70409	52.48	173.10	27	430904	570209	ATTU ISLAND	AK US	
AFU 45709	70409	52.48	173.10	28	570210	580524	ATTU ISLAND	AK US	45708
SVA 45714	70414	52.43	174.06	34	530627	590314	SHEMYA ISLAND NAVY	AK US	
SVA 45714	70414	52.43	174.06	34	530627	590314	SHEMYA ISLAND NAVY	AK US	
SVA 45714	70414	52.43	174.06	40	590315	590831	SHEMYA ISLAND NAVY	AK US	45708 45715
SVA 45715	70414	52.43	174.06	37	590831	600118	SHEMYA (WB)	AK US	45714 45709
SVA 45715	70414	52.43	174.06	38	600118		SHEMYA	AK US	
SIL 53813	72233	30.20	89.49	8	880619		SLIDELL	LA US	12884
YWA 54706	72625	45.57	77.19	130?	680699	770630	PETAWAMA	ON CN	
YWA 54706	72625	45.57	77.19	130?	770701		PETAWAMA	ON CN	
YOY 54724	71716	46.54	71.30	178?	780101		VALCARTIER	QB CN	
CFS 60701	91700	-02.46	171.43	4	450624	460199	CANTON ISLAND	HI US	60702 60703
CFS 60702	91700	-02.46	171.43	1	430517	450420	CANTON ISLAND	HI US	60701
CFS 60703	91700	-02.46	171.43	4	470507	670915	CANTON ISLAND	HI US	
GLD 93056	72465	39.22	101.82	1113	520718	570724	GOODLAND	KS US	
GLD 93056	72465	39.22	101.42	1100	570725	580531	GOODLAND	KS US	
GLD 93056	72465	39.22	101.42	1112	580601	600930	GOODLAND	KS US	
GLD 93056	72465	39.22	101.42	1113	610501	610930	GOODLAND	KS US	
GLD 93060	72269	33.11	106.29	1236	551101	610131	JALLEN SITE	NM US	23002
93061	74630?	33.48	106.40	1506	560119	610131	STALLION SITE	NM US	23002
93062	99999?	32.30	106.25	1270	600299	610106	FRYE SITE	NM US	23002
NID 93104	74612	35.41	117.41	676	450201	551103	INYOERN/CHINA LAKE	CA US	ALSO 93060, 23039, 23037
NID 93104	74612	35.41	117.41	677	551104	640531	INYOERN/CHINA LAKE	CA US	3120

Station History for North American Upper-air Stations

NID 93104	74612	35.41	117.41	677	640601	730431	INYOERN/CHINA LAKE NAF	CA US			
NID 93104	74612	35.41	117.41	681	730501		INYOERN/CHINA LAKE NAF	CA US			
NTD 93111	72391	34.07	119.07	8?	471102	501299	POINT MUGU NAS	CA US			
NTD 93111	72391	34.07	119.07	18	501299	590104	POINT MUGU	CA US			
NTD 93111	72391	34.07	119.07	25	580105	600331	POINT MUGU	CA US			
NTD 93111	72391	34.07	119.07	4	600401	630799	POINT MUGU	CA US			
NTD 93111	72391	34.06	119.07	4	630799	770106	POINT MUGU	CA US			
NTD 93111	72391	34.06	119.07	2	770107		POINT MUGU	CA US			
NZY 93112	72290	32.42	117.12	15	450409	521231	NORTH ISLAND/SAN DIEGO	CA US			
NZY 93112	72290	32.42	117.12	15	530101	560615	NORTH ISLAND/SAN DIEGO	CA US			3131
NSI 93116	72291	33.14	119.27	174	520916	730831	SAN NICOLAS ISLAND	CA US			
NSI 93116	72291	33.15	119.27	172	730901	810228	SAN NICOLAS ISLAND/SITE	CA US			
NSI 93116	72291	33.15	119.27	174	810301		SAN NICOLAS ISLAND/SITE	CA US			
NUC 93117	72293	33.01	118.35	56	720330	810705	SAN CLEMENTE ISLAND	CA US			
NUC 93117	72293	33.01	118.35	7	810706	820901	SAN CLEMENTE ISLAND	CA US			
LIO 93117	72293	33.01	118.35	7	810706	820901	SAN CLEMENTE ISLAND	CA US			
SNO 93197	72288	34.01	118.27	38	560417	650831	SANTA MONICA/CLOVER FLD	CA US			
VBG 93214	72392	34.43	120.34	123	580701	581130	VANDENBERG AFB	CA US			
VBG 93214	72392	34.43	120.34	104	581201	591221	VANDENBERG AFB	CA US			
VBG 93214	72392	34.45	120.34	98	591222	600321	VANDENBERG AFB	CA US			
VBG 93214	72392	34.45	120.34	99	651015	651202	VANDENBERG AFB	CA US			
VBG 93214	72393	34.45	120.34	100	651203		VANDENBERG	CA US			
VBG 93214	72393	34.45	120.34	113	590701	651031	POINT ARGUELLO	CA US			
PCU 93215	72392	34.40	120.35	113	590701	651031	POINT ARGUELLO	CA US			
BAB 93216	72483	39.08	121.26	34	590701	660228	SACRAMENTO/BEALE AFB	CA US			
HGT 93218	72396?	36.00	121.14	317	650628	811299?	JOLON	CA US			93221
VBG 93219	74606	34.43	120.37	26	660801	700331	VANDENBERG/BOATHOUSE	CA US			
VBG 93220	72393	34.33	120.32	63	670501	700831	VANDENBERG SOUTH	CA US			
VBG 93220	72393	34.33	120.32	63	670501	700831	VANDENBERG SOUTH	CA US			
VBG 93220	72393	34.33	120.32	101	690305	691130	VANDENBERG/SUDDEN RANCH	CA US			
VBG 93222	74504	37.30	122.30	43	651105	700527?	PILLAR POINT	CA US			
VBG 93222	74504	37.30	122.30	43	959999		PILLAR POINT	CA US			
VBG 93223	74606	34.40	120.35	112	650901		VANDENBERG AFB S	CA US			
VBG 93223	74606	34.40	120.35	112	650901		VANDENBERG AFB S	CA US			
HAT 93229	72304	35.16	75.33	88	561001	601010	SILVER HILL	MD US			13743 93734
IAD 93234	72403	38.59	77.28	85	601011		CAPE HATTERAS	NC US			13745
WAL 93739	72402	37.51	75.29	3	631014	691031	STERLING(WASH DULLES)	VA US			93722
WAL 93739	72402	37.51	75.29	4	661101	840531	WALLOPS ISLAND	VA US			13737
WAL 93739	72402	37.51	75.29	13	840601		WALLOPS ISLAND	VA US			
WAL 93739	72402	37.56	75.29	13	840601		WALLOPS ISLAND	VA US			
NJM 93743	72309?	34.41	77.01	7	70205	700423	BOGUE FLD MCALF/SWANSBO	NC US			
ACY 93755	72407	39.45	74.40	23	80903		ATLANTIC CITY	NJ US			94789
TLH 93805	72214	30.23	84.22	25	910612		TALLAHASSEE	FL US			12832
HTS 93818	72425	38.25	82.30	172	410716	480831	HUNTINGTON	WV US			3860
L00 93821	72423	38.11	85.44	166	431124	460329	LOUISVILLE	KY US			
NPA 93829	72222	30.21	87.16	3	450201	510499	PENSACOLA	FL US			93859
NPA 93829	72222	30.20	87.16	3	510499	521199	PENSACOLA	FL US			
NPA 93829	72222	30.21	87.16	3	521199	550522	PENSACOLA	FL US			3855
NIP 93837	72206	30.14	81.41	3	430601	551031	JACKSONVILLE/NAS	FL US			13889
NPA 93859	72222	30.25	87.13	27	381201	441199	PENSACOLA	FL US			93829
AKO 94005	72469?	40.07	103.10	9	690821	710425	MISS TEST SITE/BAY ST LO	MS US			12884
SNY 94007	72563	41.13	103.06	1408	520716	520526	AKRON DET R2	CO US			
CGW 94008	72768	48.13	106.37	695	551001	551121	GLASGOW	MT US			24034
CGW 94008	72768	48.13	106.37	695	551122		GLASGOW	MT US			
FCS 94018	72468	38.42	104.46	1789	690299		FORT CARSON/ARMY	CO US			
YOL 94108	71874	49.38	112.48	920	999999		LEATHERIDGE	AB CN			
UIL 94240	72797	47.57	124.33	58	660802	661009	QUILLAYUTE	WA US			24240
UIL 94240	72797	47.57	124.33	56	661010		QUILLAYUTE	WA US			
MOI 94620	71603	43.52	66.03	9	880901		YARMOUTH	NS CN			14693
LW 94789	74486	40.40	73.47	5	580918	640331	NEW YORK/IDLEWILD	NY US			
JFK 94789	74486	40.39	73.47	13	640401	730315	NEW YORK/JFK INT AP	NY US			
JFK 94789	74486	40.47	73.46	8	730316	800902	NEW YORK/FT TCTTEN	NY US			
PIT 94823	72520	40.30	80.13	375	520915	561130	PITTSBURGH/PITTSBGH AP	PA US			
PIT 94823	72520	40.30	80.13	353	561201	631004	PITTSBURGH/PITTSBGH AP	PA US			
PIT 94823	72520	40.32	80.14	361	631005	640107	PITTSBURGH/CORAPOLIS	PA US			
PIT 94823	72520	40.32	80.14	359	640108	700112	PITTSBURGH/MOON TOWNSHIP	PA US			
PIT 94823	72520	40.32	80.14	360	700213		PITTSBURGH/MOON TOWNSHIP	PA US			
BFL 94829	72539	42.15	85.10	273	540516	541002	BATTLE CREEK/FT CUSTER	MI US			
DTW 94847	72537	42.14	83.19	201	410719	420114	DETROIT/METRO	MI US			14853 14849

3158 2 SITES USED

72293 ALSO MIRAMAR
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23129 23174

OPS SIMULT W/93223
RENAMED VANDENBURG

93215 23273 93214

93221

HAVE SEEN GTS OBS 890124-
OBS SIMUL W/93214

93219 93214

wban 93738 never used

13743 93734

CURRENT LISTED WMO #

dup dat w/24032 551001-26

W PPBB ONLY

SAME WBAN AS JFK

93755 14762

Station History for North American Upper-air Stations

STATION	TIME	COORDINATES	STATION NAME	STATION TYPE	STATUS	REMARKS			
SBN 94848	72535	41.42	86.19	237	590529	590831	SOUTH BEND	IN US	
SBN 94848	72535	41.42	86.19	234	600604	600916	SOUTH BEND	IN US	
SBN 94848	72535	41.42	86.19	237	610601	610930	SOUTH BEND	IN US	
HON 94913	72654	44.23	98.18	394	530601	530930	HURON/HOWES APT	SD US	SEVERE WX SEASON ONLY
HON 94913	72654	44.23	98.13	392	540516	541002	HURON/HOWES APT	SD US	
HON 94913	72654	44.23	98.13	392	550515	590527	HURON/HOWES APT	SD US	
HON 94913	72654	44.23	98.13	398	590528	610925	HURON/HOWES APT	SD US	
ALO 94914	72548	42.33	92.24	264	530601	530930	WATERLCO	IA US	14936
ALO 94914	72548	42.33	92.24	255	590528	590930	WATERLCO	IA US	94922
CID 94917	72545	41.53	91.43	263	540516	550911	CEDAR RAPIDS	IA US	
CID 94917	72545	41.53	91.37	265	600520	610930	CEDAR RAPIDS	IA US	
OMA 94918	72553	41.22	96.01	403	540916	740129	N OMAHA	NE US	14942
OMA 94918	72553	41.22	96.01	400	740130	891231	N OMAHA	NE US	
OVN 94918	72553	41.22	96.01	400	900101		N OMAHA	NE US	
YLO 94921	72853	49.49	99.39	382	600899	650999	SHILO/CAMP SHILG	MB CN	CHANGED CALL LETTERS
YLO 94921	72853	49.49	99.23	358	650599	650999	SHILO/CAMP SHILG	MB CN	
YLO 94921	72853	49.49	99.39	382	650599	710299?	SHILO/CAMP SHILG	MB CN	
YLO 94921	72853	49.49	99.39	382	999999		?SHILO	IA US	94914
C25 94922	99999?	42.41	92.29	307	570601	640731	WAVERLY	ND US	
RDR 94925	72465	47.57	97.22	276	600614	640731	GRAND FORKS AFB	ND US	
999999?	99999?	50.39	127.35	14?	440599	450899	COAL HARBOUR	BC CN	
10010	72434	38.37	90.11	139	690414	730427	ST. LOUIS/ARCH SITE (EMS)	MO US	TO PORT HARDY
10011	72434	38.46	90.14	161	700612	701202	ST. LOUIS/MOBILE SITE (EM)	MO US	
10013	72434	38.45	90.23	172	700524	710514	ST. LOUIS/MOBILE SITE (EM)	MO US	
MDW 10020	72534	41.28	87.45	188	690414	791001	CHICAGO/MIDWAY AP (EMS)	IL US	
MDW 10021	72534	41.26	87.59	216	700611	701217	CHICAGO/MIDWAY AP (EMS)	IL US	
10030	72405	38.51	77.02	25	690516	730511	WASHINGTON (EMS)	DC US	
10031	72405	38.51	77.02	3	700710	710420	WASH/SITE 1 (EMS)	DC US	
10032	72405	38.53	77.04	20	701006	701013	ARLINGTON/SITE 3 (EMS)	VA US	
10033	72405	38.48	77.02	3	710519	999999	WASH/ALEXANDRIA MARINA	DC US	
10034	72405	38.54	77.01	15	701026	999999	WASH/CAMP STN/SITE 1 (EM)	DC US	
10035	72405	38.51	76.56	88	710708	711015	WASH/SITE 5 (EMS)	DC US	
LGA 10040	72503	40.46	73.54	13	690617	720612	NY/LAGUARDIA AP (EMS)	NY US	
LGA 10041	72503	40.46	73.59	33	700611	700819	NY/CENTRAL PARK SITE (EM)	NY US	
PHL 10050	72408	39.53	75.11	5	690627	711130	PHILADELPHIA (ENSU)	PA US	
PHL 10051	72408	39.53	75.11	6	711201	790799	PHILADELPHIA (ENSU)	PA US	
PHL 10051	72408	39.53	75.11	5	690627	700628	PHILADELPHIA (ENSU)	PA US	
PHL 10052	72408	40.00	75.13	79	700611	701110	PHILADELPHIA (ENSU)	PA US	
PHL 10053	72408	39.59	75.06	3	700723	710902	PHILADELPHIA (ENSU)	PA US	
CLE 10060	72424	41.30	81.36	217	710401	730327	CLEVELAND (EMS)	OH US	
10070	72423	38.12	85.45	141	710429	730615	LOUISVILLE (EMS)	KY US	
DEN 10080	74530	39.47	104.59	1576	710423	730408	DENVER (EMS)	CO US	
DEN 10080	74530	39.46	104.53	1611	730409	730629	DENVER (EMS)	CO US	
EMT 10090	74704	34.05	118.02	91	710401	720102	EL MONTE (EMS)	CA US	
EMT 10090	74704	34.05	118.02	92	720103	791001	EL MONTE (EMS)	CA US	
LAX 10100	72295	33.56	118.23	34	710501	790930	LOS ANGELES (EMS)	CA US	
10110	74505	37.19	121.52	32	710630	730608	SAN JOSE (EMS)	CA US	
400?10111	74505	37.56	121.41	21	720609	720623	SAN JOSE/BRENTWOOD (EMS)	CA US	(9 SOUNDINGS)
10112	74505	38.27	122.43	45	720906	720908	SAN JOSE/SANTA ROSA (EMS)	CA US	(5 SOUNDINGS)
10120	72509	42.21	71.05	30	710824	730426	BOSTON (EMS)	MA US	
EFD 10130	72443	29.46	95.22	17	710816	770207	HOUSTON (EMS)	TX US	
EFD 10130	72443	29.46	95.22	12	770823	790630	HOUSTON (EMS)	TX US	
10140	72793	47.39	122.18	8	711018	730701	SEATTLE (EMS)	WA US	
BFI 10141	72793	47.32	122.18	4	710915	711017	SEATTLE/BOEING FLD (EMS)	WA US	
PIT?10150	74719	40.26	80.00	224	711115	730513	PITTSBURGH (EMS)	PA US	
10160	72337	42.19	83.13	187	720703	730328	DETROIT (EMS)	MI US	
CRW 10170	72414	38.23	81.46	182	720727	791129	CHARLESTON (EMS)	WV US	
BHM 10180	72428	33.34	86.45	190	720801	781005	BIRMINGHAM (EMS)	AL US	
BHM 10180	72428	33.28	86.50	227	781016	800829	BIRMINGHAM (EMS)	AL US	
10190	72498	45.32	122.41	42	721030	730618	PORTLAND (EMS)	OR US	

APPENDIX B(3)

Station Equipment History for North American Upper-air Stations

DRA	3109	72387	3	G2	510811	G3	520429	G4	550201															
NID	3120	72388	2	G3	540617	G4	580909																	
FHU	3124	72273	2	G4	550105	H1	610203																	
YUM	3125	72280	4	G4	540511	H1	610606	G3	650601	H1	650601													
SAN	3131	72290	12	G3	560616	G4	570413	S2	650722	H1	651215	C2	691108	H3	720609									
					C3	750128	M3	790716	H4	810121	S3	810821	C5	861113	S4	881004								
TFH	3132	72485	1	G4	560920																			
UCC	3133	72385	6	G4	560915	H1	661001	G5	681015	C2	710822	H3	720413	C3	770127									
???	3134	99999	1	G3	570422																			
???	3143	72385	3	G4	590429	G4	600526	G4	610420															
NJK	3146	72281	1	G4	620228																			
NSI	3158	72291	1	G5	730901																			
DRA	3160	72387	5	G5	780516	C3	780516	C5	860422	C6	860828	S4	881004											
PNS	3855	72222	2	G4	570107	H1	610403																	
HTS	3860	72425	11	G8	611201	S2	650414	H1	651223	C2	710313	H3	720317	C3	750304									
					S2	650414	S3	810821	H4	810821	C6	860708	S4	881009										
SLO	3879	72433	10	G4	690819	C2	690924	H3	720120	G8	750403	C3	760605	M3	790301									
					S3	801101	H4	801101	C6	861025	S4	881007												
CKL	3881	72229	8	G7	741116	C2	741116	H1	741116	C3	741217	H4	810123	S3	810715									
					C6	860408	S4	881031																
FSM	3926	72344	2	G2	530317	G4	530423																	
LCH	3937	72240	8	G8	611230	H1	651231	C2	720114	H3	720129	S3	801031	H4	801031									
					C6	860821	S4	881019																
JAN	3940	72235	7	C2	711028	H3	720120	C3	760602	S3	810722	H4	810722	C6	860506									
					S4	880901																		
UMN	3946	72349	9	G8	700905	S2	700905	C2	700905	H3	720620	C3	760123	H4	810403									
					S3	810707	C6	861108	S4	881008														
OUN	3948	72357	2	G8	740101	C2	740101																	
GGG	3951	72247	8	G4	750713	C2	750713	C3	760408	S3	801109	H4	801109	C4	840704									
					C6	860411	S4	881025																
1M1	3952	72340	4	S3	810606	H4	810606	C6	860506	S4	880901													
YMW	4734	72722	2	G2	530701	G3	650525																	
IAG	4738	72528	1	G4	540315																			
???	L0010	72434	1	H3	720810																			
???	L0030	72405	1	H3	720502																			
PHL	L0050	72408	1	H3	720811																			
CLE	L0060	72524	2	H1	710401	H3	720626																	
???	L0070	72423	1	H3	720526																			
DEN	99999	74530	1	C2	730409																			
EMT	L0090	74704	3	H3	720526	C2	780920	M3	781215															
LAX	L0100	72295	2	H3	720722	C2	781002																	
???	L0110	74505	1	H3	720426																			
???	L0120	72509	1	H3	720419																			
EFD	L0130	72243	2	H1	710816	H3	720501																	
???	L0140	72793	1	H3	720731																			
PIT	L0150	74479	1	H3	720518																			
???	L0160	72537	2	H3	720703	M2	721101																	
CRW	L0170	72414	1	H1	720727																			
BHM	L0180	72228	1	H3	720801																			
???	L0190	72698	1	H3	721030																			
BLB	10701	78806	3	G2	471220	G4	531118	H1	611201															
BDI	11501	78954	8	G5	650730	H1	650730	H3	720510	M2	721101	C3	810514	M1	810514									
					C5	999999	S4	881020																
ANU	11604	78861	1	G2	450710																			
???	11608	78526	1	G2	440505																			
CGU	11610	78967	1	G2	490527																			
CGU	11621	78967	3	G4	531209	H1	610516	G5	620101															
SDQ	11629	78486	6	G2	620806	H1	651124	H2	660810	H2	670103	G4	700524	G4	750525									
???	11631	78526	2	G2	451210	G2	491109																	
KPP	11634	78970	2	G5	691212	H3	720301																	
SIG	11636	78526	1	G2	500201																			
JSJ	11641	78526	10	G2	550524	G2	550701	G7	610907	S1	631212	H1	631212	H3	720129									
					C3	740828	S3	801120	H4	801120	S4	881006												
FFR	11642	78897	4	G2	560221	H1	650817	G4	680311	H3	720516													
ACC	11643	78988	4	G2	560605	H1	650729	G4	700522	H3	720401													
ACM	11645	78866	5	G2	561002	H1	650817	G5	700517	H3	720321	M2	720907											

APPENDIX B(3) (Continued)

Station Equipment History for North American Upper-air Stations

SDM	11646	78467	1	G2	560919														
KPA	11647	78861	2	G4	570901	G6	690310												
KJP	11704	78397	1	G2	450718														
UGM	11706	78367	4	G4	540722	H1	610213	G5	611004	M2	730224								
KJP	11715	78397	4	G2	560903	H1	650623	G5	700423	H3	720314								
SWA	11807	78501	6	G2	540923	G4	601123	H1	650528	S1	680101	H3	720518	C3	760120				
KCR	11813	78384	8	G2	560814	H1	650906	G4	700919	H3	720404	M2	730218	C3	760221				
				H4	801224	S4	880901												
GUA	11901	78640	4	G4	731108	H1	731108	H3	731108	M2	740125								
MEX	11903	76679	4	G0	430210	G2	610111	M2	721001	G4	731213								
VER	11904	76692	4	G2	610219	H1	660304	H3	720214	M2	721001								
CMW	12711	78355	1	G2	531203														
YGM	12712	78063	2	G4	610125	G6	690310												
YEM	12713	78076	2	G3	520215	G6	690310												
KJT	12714	78118	2	G4	541116	G6	690310												
???	12715	78107	1	G3	551010														
YSM	12716	78089	1	G4	560112														
NAS	12717	78073	4	G3	771214	C3	771214	S3	801225	H4	801225								
MIA	12829	72202	1	G1	450620														
AQQ	12832	72220	7	G5	740701	C2	740701	C3	751202	S3	801118	H4	801118	C5	860520				
				S4	881001														
MIA	12839	72202	8	G1	460122	G2	461001	G7	591201	H1	630208	S1	630208	C2	710205				
				H3	720214	C3	740508												
TPA	12842	72210	13	G0	430526	G2	540114	G4	600719	H1	631007	H1	651204	C2	710925				
TBW				H3	720104	C3	740924	C3	750627	S3	801024	H4	801024	C5	860609				
				S4	881001														
PBI	12844	72203	6	G7	770303	C3	770303	S3	801030	H4	801030	C6	860616	S4	881001				
EYW	12850	72201	11	G4	540501	G5	601201	H1	610301	C4	610901	C5	640219	C2	720629				
				H3	720629	S3	801031	H4	801031	C5	860604	S4	881011						
	12863	72232	5	G2	460224	G2	500815	G4	600217	H1	630927	S1	630927						
HAV	12864	78325	1	G2	500401														
COF	12867	74794	3	G2	500204	G3	510408	G4	530205										
XMK	12868	74794	2	G4	561118	G6	690310												
MID	12878	76644	5	G2	561007	H1	650907	H3	720215	M2	721001	G3	761001						
CSB	12879	72224	1	G4	601227														
	12880	99999	1	G4	601223														
	12881	99999	1	G4	620299														
BVE	12884	72232	10	G8	650213	S1	650213	H1	650213	G8	660101	S2	670217	H2	680208				
				S2	710426	H3	720106	C3	740716	M3	790715								
EFD	12906	72243	1	G4	530399														
VCT	12912	72255	9	G7	660701	H1	660701	H3	720111	C2	720409	C3	761015	S3	801110				
				H4	801110	C6	860821	S4	881003										
MSY	12916	72231	1	G2	461218														
BRO	12919	72250	10	G0	400805	G2	460510	G7	600511	H1	630815	S1	630815	S1	671201				
				C2	710822	C3	770120	C6	860722	S4	881001								
SAT	12921	72253	3	G2	451112	G7	610308	H1	660113										
NGP	12926	72251	5	G3	530201	G3	540828	G4	550919	H1	610401	G5	621204						
SIL	12930	72233	4	C3	880622	S3	880622	H4	880622	S4	881006								
???	12958	72231	1	G4	650921														
XKF	13601	78016	4	G1	440517	G2	450714	G4	530310	M2	721201								
ADW	13705	72403	1	G1	490726														
GSO	13723	72317	10	G2	480311	G7	600417	H1	650412	C2	710119	H3	720101	C3	750128				
				S3	801115	H4	801115	C6	860529	S4	881031								
ORF	13737	72308	2	G4	551115	S2	650429												
???	13739	72408	1	G3	550101														
DCA	13743	72405	1	G0	340799														
HAT	13745	72304	2	G2	460223	G4	560916												
NGU	13750	72308	2	G2	461201	G4	520609												
NDY	13760	74574	1	G4	540113														
GUN	13801	72226	1	G4	541218														
BLV	13802	72433	2	G1	500705	G4	540516												
BYH	13814	72340	2	G4	570301	G4	630322												
NAB	13815	72216	3	G4	560215	G4	590215	G4	600201										
MXF	13821	72226	3	G1	450124	G2	460322	G4	530509										
DAY	13840	72429	11	G2	510901	G4	530211	H1	650408	S2	650922	C2	700120	C1	700424				
				H3	720322	C3	750211	M3	800915	C5	861110	S4	881101						

APPENDIX B(3) (Continued)

Station Equipment History for North American Upper-air Stations

ILN	13841	72721	1	G2	461001													
TOL	13849	72536	1	G0	440104													
VPS	13858	72221	3	G1	451201	G2	471127	G4	521220									
WRB	13860	72217	2	G2	481115	G4	540102											
AYS	13861	72213	8	G7	690415	C2	700916	H3	720104	C3	760316	S3	801109	H4	801109			
					C6	860522	S4	881025										
MEM	13862	72334	2	C3	530307	C4	540201											
AHN	13873	72311	11	G3	550904	G2	571004	G7	590630	H1	650319	C2	710224	H3	711231			
					C3	750507	S3	801109	H4	801109	C6	860909	S4	881018				
ATL	13874	72219	2	G1	491214	G3	540226											
CHS	13880	72208	13	G0	390714	G2	470421	G3	571003	G7	590826	S2	650203	H1	651111			
					C2	701006	H3	720321	C3	741119	S3	810701	H4	810701	C6	860221		
					S4	881023												
JAX	13889	72206	5	G4	551101	H1	650617	S1	650617	S2	660123	H1	650617					
MGM	13895	72226	9	G4	560601	G7	591106	S2	650105	H1	650428	H2	660204	H1	660227			
					G4	560601	C2	720415	H3	720503								
BNA	13897	72327	14	G0	380713	G2	460213	G3	600201	G8	640315	S1	650411	S2	650416			
					H1	650419	C2	690923	H3	720399	C3	760111	H4	810221	S3	810710		
					C6	860622	S4	880901										
SEP	13901	72260	6	G4	731103	C2	731103	C3	741904	H4	810109	C5	860205	S4	881011			
LTS	13902	72352	1	G4	540201													
???	13905	72244	1	G3	540201													
END	13909	72353	1	G2	500316													
DYS	13910	72266	1	G4	570301													
FWH	13911	72259	8	G2	480823	G4	521211	H1	650312	H2	650813	H1	651006	S2	651022			
					C2	700803	H3	720516										
FOE	13920	72456	2	G4	531221	G4	540202											
FLV	13921	72457	2	G2	461022	G4	530305											
SLN	13922	72458	3	G1	440799	G2	530301	G4	530617									
HKS	13927	72235	2	G3	530301	C4	550215											
???	13928	72256	2	G3	510117	G2	520307											
LCH	13941	72240	3	G0	999999	G2	530301	G3	600519									
BAD	13944	72248	2	G2	480824	G3	520117											
BAD	99999	72248	1	G4	530926													
FSI	13945	72355	2	G3	520219	G4	600215											
FRI	13947	72455	1	G3	580404													
HKS	13956	72235	5	G7	600731	S2	650101	H1	650904	H2	660701	H1	660816					
SHV	13957	72248	5	H1	630423	S1	630423	S1	671201	C2	720112	H3	720120					
ABI	13962	72266	4	G3	630204	H1	650302	H3	720201	C2	730201							
LIT	13963	72340	9	G0	999999	G2	460621	G4	610126	G8	631121	S2	641229	H1	651129			
					C2	710827	H3	720816	C3	750710								
OKC	13967	72353	10	G0	380717	G2	470205	G7	591218	H1	650306	G3	750107	C3	750114			
					H4	810119	S3	810707	C5	860812	S4	880925						
COV	13983	72445	5	G2	460202	G3	531206	G7	610406	S2	650216	H1	650428					
DDC	13985	72451	10	G2	530319	G7	600411	H1	650403	C2	710114	H3	720125	C3	750911			
					S3	801103	H4	801103	C6	860820	S4	881013						
TOP	13996	72456	11	G4	550930	G8	610221	H1	650405	H3	720121	C2	730124	C3	760107			
					S3	801101	H4	801101	C4	840407	C6	860724	S4	881001				
YQX	14501	72803	1	G1	431208													
YJT	14503	72815	2	G2	450924	G4	520924											
YYT	14505	74198	1	G2	500608													
YAR	14508	72807	3	G5	520701	G4	630508	H1	610131									
YQX	99999	72803	1	G1	431208													
YYT	14531	71801	1	G3	710427													
PQI	14604	72713	1	G2	450401													
CAR	14607	72712	14	G0	420403	G2	460799	G4	550801	S1	650612	H1	650627	S2	651030			
					S1	671299	C2	711207	H3	720213	C3	740806	H4	810919	C4	840519		
					C6	860820	S4	881020										
NHZ	14611	74392	1	G3	530303													
YSA	14642	72600	2	G2	540212	G3	650622											
CHH	14684	74494	10	S2	701118	S1	710114	C2	710722	H3	720429	C3	740604	H4	810226			
					S3	810930	C4	840599	C6	860625	S4	881101						
YCX	14685	72701	2	G3	710199	G3	720501											
WOS	14688	74399	1	G3	721101													
AGC	14701	72520	1	G2	440829													
WY9	14708	74498	2	G1	500209	G2	520322	G4	530211									

APPENDIX B(3) (Continued)

Station Equipment History for North American Upper-air Stations

SWF	14714	74482	2	G2	470516	G2	500318											
RME	14717	72518	3	G2	470520	G3	520808	G4	530701									
PWM	14724	72606	1	G1	440104													
BUF	14733	72528	11	G0	390901	G4	600820	H1	650406	C2	710824	H3	720101	C3	751104			
				M3	800901	S3	801109	H4	811109	C5	860731	S4	881024					
ALB	14735	72518	11	G4	551019	H1	650315	H2	650512	H1	651114	C2	710928	H3	720110			
				C3	741031	S3	810811	H4	810811	C5	860419	S4	880901					
ACK	14756	72506	7	G0	460416	G2	461113	G7	591211	S2	650512	S1	650605	H1	650619			
				S1	680101													
PWM	14764	72606	11	G4	550608	G3	551001	G8	611229	H1	651204	C2	700225	H3	720120			
				C3	750923	S3	801112	H4	801112	C6	860923	S4	881101					
MTC	14804	72537	2	G2	451201	G3	520623											
RAN	14806	72531	3	G1	440902	G2	470199	G4	530326									
???	14809	72520	2	G1	450301	G2	510801											
FNT	14826	72637	13	G4	560919	G8	610127	S2	650107	H1	650508	H2	660117	H1	660419			
				H3	720203	C2	730816	C3	760710	S3	810715	H4	810715	C6	860721			
				S4	881003													
JOT	14834	72534	1	G0	390701													
PIA	14842	72532	14	G4	560912	G8	610506	S2	650121	H1	650121	S1	650121	H1	650501			
				S1	680101	C2	710330	H3	720513	C3	760619	H4	810127	S3	810629			
				C6	860926	S4	881001											
SSM	14847	72734	15	G2	461005	G4	531206	G8	610119	S2	650210	S1	650210	H1	650604			
				S1	680101	C2	710723	H3	720313	C3	740409	H4	810225	S3	810707			
				H4	810225	C6	860603	S4	881005									
TOL	14849	72536	1	G0	440104													
GRB	14898	72645	10	G2	530317	G7	600302	H1	651120	C2	700303	H3	720123	C3	750129			
				S3	801101	H4	801101	C6	860529	S4	880901							
INL	14918	72747	12	G2	461115	G3	541004	G7	600125	H1	630405	S1	630405	S1	670799			
				H3	720202	C3	740626	S3	801105	H4	801105	C6	861202	S4	881030			
STC	14926	72655	9	G2	481099	G7	600222	S2	650225	H1	650229	H3	720101	C2	730301			
				C3	751118	C6	860611	S4	881101									
HON	14936	72654	11	G3	630606	G4	640601	H1	650604	C2	720502	H3	720505	M2	730601			
				C3	740731	S3	801107	H4	801107	C6	861205	S4	881001					
OMA	14942	72553	1	G2	380716													
OFF	14949	72553	1	G1	501204													
YJR	15601	72816	4	G1	440399	G2	450303	G2	460601	G3	521203							
YLP	15604	74188	2	G2	450899	G2	470799											
YVP	15605	72906	1	G2	490899													
YZV	15613	72811	2	G2	520199	G3	680128											
YNI	15703	72826	2	G2	560299	G3	700226											
YPH	15704	72907	2	G2	540499	G3	660217											
YMO	15803	72836	2	G2	530499	G3	661204											
YTL	15806	72848	2	G2	530213	G3	660903											
YYQ	15901	72913	3	G2	470199	G2	490199	G3	610799									
YFB	16603	72909	3	G2	451099	G2	500999	G3	651199									
YZS	16801	72915	2	G2	541011	G3	651002											
YUX	16895	72031	2	G2	570899	G3	640909											
YBK	16903	72926	2	G2	541119	G3	650719											
YCY	17601	74090	2	G2	481099	G3	661004											
YRB	17901	71924	1	G2	471024													
YLT	18601	74082	2	G2	500910	G4	600219											
YEU	18801	72917	2	G2	470918	G3	611001											
???	21001	76654	1	G5	760717													
SIC	21101	76723	2	G2	731016	G5	760427											
ITO	21504	91285	10	G2	500218	G4	610713	H1	650227	C2	700801	H3	720502	C3	740518			
				S3	801025	H4	801025	C5	999999	S4	881015							
DLF	22001	72261	1	G4	540128													
MCV	22007	76225	5	G4	640805	G4	650525	G4	670701	H3	720328	M2	721001					
MZT	22009	76458	4	G2	640129	H1	660210	H3	720415	M2	721001							
DRT	22010	72261	9	G8	630304	S2	650126	H1	651112	H3	720102	C3	750415	S3	801101			
				H4	801101	C6	860520	S4	881001									
MTY	22012	76394	4	G4	641001	H1	650706	H3	720410	M2	721001							
???	22013	76612	1	G5	790301													
GYM?	22104	76256	5	G4	641122	G4	650205	H1	650719	H3	720313	M2	721001					
IGP?	22105	76151	5	G2	710116	H1	710116	H3	720307	M2	721101	G5	740227					
BKH	22501	91162	1	G5	630801													

APPENDIX B(3) (Continued)

Station Equipment History for North American Upper-air Stations

HIK	22504	91182	1	G1	440109	G2	450701												
LIH	22536	91165	12	G2	500514	G4	600526	H1	630611	S1	630611	S1	680101	C2	710601				
				H3	720611	C3	741112	S3	801125	H4	801125	C5	999999	S4	881016				
BKH	22545	91162	2	G5	650802	G5	670626												
HMN	23002	72269	2	G2	480301	G4	520702												
AMA	23003	72363	1	G2	520215	G4	530214												
LKY	23012	72469	1	G4	531115														
GOF	23017	72263	1	G4	640120														
ELP	23019	72270	1	G1	440617														
REE	23021	72267	2	G3	520215	G4	600315												
MAF	23023	72265	11	G2	531115	G7	600421	H1	630404	S1	630404	C2	691030	H3	711229				
				C3	760415	S3	801112	H4	801112	C6	860624	S4	881014						
???	23037	99999	1	G2	460523														
???	23038	99999	1	G2	480323														
???	23039	72269	4	G2	461107	G1	480518	G3	530106	G4	531017								
HCA	23041	72265	1	G2	451209														
ELP	23044	72270	11	G0	390712	G2	550325	G7	600801	H1	651207	H3	720125	C2	720220				
				C3	741121	S3	801105	H4	801105	C6	860911	S4	881001						
AMA	23047	72363	8	H1	650415	C2	711207	H3	720119	C3	760209	S3	801219	H4	801219				
				C5	860325	S4	881001												
ABQ	23050	72365	13	G2	460109	G7	600530	S2	650106	H1	651124	H2	660924	H1	660999				
				C2	700707	H3	720406	C3	750510	H4	810208	S3	810713	C6	860909				
				S4	881001														
DEN	23062	72469	10	G4	560815	G8	610126	H1	650406	C2	710914	H3	720105	C3	760318				
				S3	801111	H4	801111	C6	860828	S4	881001								
GJT	23066	72476	12	G2	460910	G7	591103	S2	641217	S1	641217	H1	650507	C2	711027				
				H3	720317	C3	740501	H4	810318	S3	810614	C6	861019	S4	881019				
DMA	23109	72274	2	G2	450721	G4	511204												
LSV	23112	72386	1	G4	450799														
EDW	23114	72381	3	G2	500308	G3	520211	G4	530924										
RAA	23118	72488	3	G4	531015	G4	550201	G4	550208										
TPH	23128	72485	2	G3	511008	G4	550201												
LGB	23129	72297	2	G2	470310	G4	530401												
ELY	23154	72486	11	G1	390724	G2	531029	G2	540601	G7	600118	S2	650123	H1	660416				
				H3	720526	C3	760406	H4	810902	C6	860607	S4	881006						
TUS	23160	72274	12	G4	560301	S1	650610	H1	650615	S2	650722	S1	671130	C2	710111				
				H3	720518	C3	740911	H4	810219	S3	810708	C5	860205	S4	881004				
LAS	23169	72386	4	G3	540201	G4	610204	G8	640528	H1	651215								
PHX	23183	72278	1	G2	541210														
INW	23194	72374	10	G8	611101	S2	650225	H1	660108	H3	720120	C2	721205	C3	741204				
				H4	810227	S3	810817	C6	860925	S4	881004								
CIC	23201	72497	1	G5	620206														
MER	23203	72481	2	G2	501202	G4	531101												
OAK	23230	72493	13	G2	510199	G4	541002	H1	630403	S1	630403	S2	690529	C2	700120				
				H3	720312	C3	750916	M3	790618	H4	801217	S3	810201	C6	861209				
				S4	881001														
SMX	99999	72394	1	G2	460908														
BFF	24007	72566	1	G4	530601														
BIS	24011	72764	12	G2	460423	G7	591209	S2	650107	H1	650501	S1	680101	H3	720517				
				C2	720913	C3	741017	H4	810314	S3	810814	C6	860403	S4	881001				
LND	24021	72576	13	G0	450901	G2	541030	G7	591130	H1	651128	H2	660122	H1	660222				
				C2	711120	H3	720104	C3	740529	S3	801119	H4	801119	C6	861218				
				S4	881001														
LBF	24023	72562	13	G0	450106	G2	530499	G7	591201	S2	641230	S1	641230	H1	650426				
				C2	691202	H3	720605	C3	750111	H4	810305	S3	810728	C6	860514				
				S4	880901														
RAP	24026	72662	1	G2	460928														
GGW	24034	72768	1	G1	430606														
RAP	24090	72662	11	G2	501013	G4	550402	G8	610214	H1	651226	C2	700714	H3	720107				
				C3	750313	S3	801115	H4	801115	C6	861208	S4	881017						
HIF	24101	72575	3	G2	481105	G3	521206	G4	530919										
DFG	24103	72581	2	G2	491015	G4	531001												
ENV	24111	72213	1	G7	480399														
SLC	24127	72572	11	G4	560807	G8	610201	S2	650124	H1	650425	C2	690930	H3	720430				
				C3	740408	H4	810203	S3	810810	C6	860203	S4	881008						
WMC	24128	72583	9	G4	560501	G8	610304	S2	650201	H1	660219	H3	720201	C3	760519				

APPENDIX B(3) (Continued)

Station Equipment History for North American Upper-air Stations

BOI	24131	72681	14	H4 990929 G0 390901 S2 660602 C6 860409	C6 860725 G2 460305 H3 720210 S4 881015	S4 880901 G0 460999 C2 720718	G2 490729 C3 740422	G7 591218 H4 810401	H1 651203 S3 810626
GTF	24143	72775	17	G0 400801 G7 611223 S3 811114	G1 530402 S2 650127 H4 811114	G1 530999 H1 650406 C4 850509	G3 531218 H1 690101 C6 860906	G3 540599 H3 720119 S4 881025	G8 610624 C3 751202
GEG	24157	72785	11	G2 470126 C3 741105	G4 540430 H4 810201	S2 651002 S3 810703	H1 660128 C5 850726	H3 720601 S4 881004	C2 730109
TCM	24207	72793	1	G1 520404					
NEJ	24208	72793	1	G2 440901					
MFR	24209	72597	1	G2 440901					
IAP	24211	72698	2	G2 460101	G3 530202				
MFR	24225	72597	13	G2 460210 C2 700721 S4 881006	G7 591121 H3 720612	S2 650211 C3 740716	S1 650516 H4 810924	H1 650617 S3 811025	S1 680101 C6 860418
OLM	24227	72792	1	G8 620601					
SLE	24232	72694	10	G4 560601 S3 801209	G8 610312 H4 801209	H1 660104 C6 860601	C2 710601 S4 881005	H3 711231	C3 741119
SEA	24233	72793	1	G4 560629					
TTI	24240	72798	4	G2 451125	G4 541001	H1 630426	S1 630426		
NEJ	24244	72793	2	G1 450301	G4 540115				
YQD	25004	72867	2	G2 560199	G3 650831				
YXD	25111	72879	2	G2 461099	G2 531015				
WSE	25145	74119	1	G3 660215					
YVR	25152	74115	1	G2 711008					
YXS	25206	72896	2	G2 460599	G7 641022				
YYE	25218	72945	2	G2 560199	G3 650805				
YZT	25223	74109	2	G2 540419	G3 640504				
ANN	25301	70398	1	G2 440414					
YAK	25302	70361	1	G2 440818					
ANN	25308	70398	10	G7 600226 S3 801025	S1 630521 H4 801025	S1 671201 C6 860423	H1 630521 S4 881001	H3 720509	C3 751111
YAK	25339	70361	9	G2 480801 H4 801019	G7 600720 C6 860721	H1 650408 S4 881001	H3 720313	C3 740619	S3 801019
ADQ	25501	70350	8	G4 520922 C6 860514	H1 611002 S4 881001	G5 620112	C3 740502	S3 801208	H4 801208
AKN	25503	70326	9	G4 530505 S3 820903	G7 591115 C6 861113	H1 650411 S4 881001	H3 720513	C3 740411	H4 810806
???	25602	70485	1	G2 460614					
CDB	25603	70316	2	G2 451119	G3 530328				
ADU	25620	70489	1	G2 510128					
CDB	25624	70316	9	G2 550820 C3 740829	G7 600410 C6 860610	H1 630528 S4 881006	S1 630528	S1 671201	H3 720521
ADK	25701	70454	1	G1 440301	G2 460626				
ADK	25704	70454	5	G4 530616	G5 610722	G5 610722	H1 610930	M2 731128	
SNP	25713	70308	10	G2 481101 S3 801101	G7 600422 H4 801101	H1 650416 C6 860629	S1 680111 S4 881004	H3 720505	C3 740608
YCB	26005	72925	1	G3 700217					
YSM	26102	72934	3	G1 461199	G2 530299	G3 651011			
YCO	26107	72938	1	G2 570799					
YVQ	26202	74043	2	G2 550199	G3 550613				
YXY	26311	72964	1	G2 451199					
YXY	26316	72964	2	G2 461099	C3 650630				
ANC	26401	70273	1	G2 451011					
FGJ	26406	70263	2	G2 510607	G4 570614				
ANC	26409	70273	14	G0 430202 C2 710824 C6 860203	G2 460522 H3 720315 S4 881006	G7 590701 C3 740328	G7 640709 M3 801001	H1 650324 S3 801211	S1 680111 H4 801211
FAI	26411	70261	11	G2 451101 C3 740523	G7 600201 S3 801024	H1 630426 H4 801024	S1 630426 C6 860206	S1 671201 S4 881004	H3 720516
MCG	26510	70231	10	G0 420411 S3 801202	G2 561019 H4 801202	G7 600722 C6 861125	H1 650409 S4 881002	H3 720414	C3 740918
OME	26604	70200	1	G2 450301					
BET	26615	70219	8	G0 999999 C6 860930	G2 550704 S4 881001	G7 600913	H1 650404	M3 720326	C3 750601

APPENDIX B(3) (Continued)

Station Equipment History for North American Upper-air Stations

OTZ	26616	70133	10	G0	421026	G2	541015	G7	591016	H1	650406	H3	720618	C3	741211
				S3	801110	H4	801110	C6	860529	S4	881001				
OME	26617	70200	9	G7	461020	H1	650407	S1	680116	H3	720501	C3	741206	S3	801112
				H4	801112	C6	860327	S4	880901						
YIC	27001	74074	2	G2	541005	G4	611017								
YMD	27101	74072	2	G2	531022	G4	600403								
YSY	27201	74051	2	G2	551101	G3	660830								
BTI	27401	70086	11	G2	530327	G4	530822	G7	591211	H1	650425	H3	720506	M2	721022
				C3	750419	S3	801109	H4	801109	C6	861021	S4	881001		
BRW	27502	70026	11	G2	451101	G7	591112	S1	630519	S1	671211	H1	630519	H3	720423
				C3	750425	S3	991202	H4	991202	C6	860903	S4	881001		
AMC	45702	70439	2	G1	440606	G2	451105								
SYA	45708	70414	4	G1	440401	G2	451005	G2	510101	G4	521216				
ATU	45709	70409	1	G4	550614										
SYA	45715	70414	5	G4	580627	G7	600624	H1	650327	S1	680120	H3	720602		
GLD	93056	72465	2	G3	520718	G4	530601								
???	93060	72269	1	G4	560103										
???	93061	99999	1	G4	560119										
???	93062	99999	1	G4	600299										
NID	93104	74612	1	G4	640399										
NTD	93111	72391	2	G4	560905	G5	610614								
NZY	93112	72290	2	G2	510206	G3	530201								
NSI	93116	72291	4	G2	520917	G4	521204	G5	600405	H1	620125				
SMO	93197	72288	3	G4	560417	H1	650506	S2	650625						
VBC	93214	72393	5	G3	580701	C2	700701	C3	750601	S3	810109	H4	810109		
PGU	93215	72392	5	G3	590701	H3	620115	S1	640108	H1	640108	G3	650121		
HGT	93218	72396	2	G4	650628	H1	650628								
???	93722	72405	3	G2	501001	G4	530101	G7	590601						
HAT	93729	72304	11	G5	570301	S1	650529	H1	650607	G4	650804	S2	650813	C2	700712
				H3	720206	C3	740511	S3	810311	C5	860115	S4	881022		
IAD	93734	72403	12	G4	601011	G4	610101	G8	620110	S2	650316	H1	650316	C2	701009
				H3	720213	C3	740416	H4	801221	S3	810702	C6	860910	S4	880901
WAL	93739	72402	8	G5	631014	S1	631014	H1	650803	C2	720417	G9	740518	C3	750314
				M3	791001	H4	830127								
ACY	93755	72407	6	C3	800903	G7	800903	S3	801111	H4	801111	C6	860718	S4	881027
HTS	93818	72425	1	G2	460199										
NIP	93837	72206	2	G3	530117	G4	530401								
???	93868	74768	1	G3	690821										
SNY	94007	72563	1	G3	550515										
GGW	94008	72768	11	G1	551026	G2	551027	G2	551122	G7	600229	H1	650430	H3	720116
				C3	760303	S3	991111	H4	991111	C6	860626	S4	880901		
UIL	94240	72797	11	G4	660802	H1	660802	S1	660802	G8	661211	H3	720113	C3	760914
				S3	801106	H4	801106	M3	810701	C6	861017	S4	881029		
JFK	94789	74486	11	G4	560918	H1	650320	S2	650719	S2	650719	H2	650831	H1	651010
				C2	690101	H3	711229	G9	730316	C3	770621	M3	790827		
PIT	94823	72520	14	G1	520915	G4	540427	G8	631005	S2	650108	S1	650202	H1	650402
				S1	680101	C2	691007	H3	720312	C3	760106	S3	810716	H4	810716
				C6	860821	S4	881001								
SBN	94848	72535	3	G4	590529	G4	600604	G4	610601						
HON	94913	72654	2	G4	530601	G4	600615								
ALO	94914	72548	2	G4	530601	G4	590528								
CID	94917	72545	1	G4	540599										
OMA	94918	72553	12	G3	540916	G4	590202	G3	600612	G8	610304	H1	650404	H3	720113
				C2	730106	C3	760224	S3	801105	H4	801105	C6	860201	S4	880901

APPENDIX C

Example of the Hydrostatic Checking and Correction Computer Procedure

NOTE: The complete code is available by contacting Barry Schwartz at (303)497-6481, or in writing at: NOAA/ERL/FSL, Mail Code: R/E/FS1, 325 Broadway, Boulder, CO 80303.

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PROGRAM HYCHECK
IMPLICIT NONE

CCCCC
C      1. REARRANGED BY XIAOPING ZHONG ON MAR. 17, 1989.
C      2. MAIN PROGRAM HAS BEEN MODIFIED BY XIAOPING ZHONG ON MAR. 19, 1989.
C-----
CCCCC  PURPOSE:
C      THIS ROUTINE READS KANSAS CITY FORMATTED RADIOSONDE DATA
C      USING SUBROUTINE READKC.  MANATORY DATA IS EXTRACTED FROM THE
C      RADIOSONDE AND CHECKED HYDROSTATICALLY BY COMPUTATION OF
C      DELTAS.  DELTAS ARE COMPARED AND HYDROSTATIC CORRECTIONS ARE
C      PERFORMED WHERE POSSIBLE.  IN ADDITION, THIS ROUTINE WILL
C      CALL SUBPROGRAMS TO COMPUTE MISSING 1000 AND 850 MB HEIGHTS
C      FOR STATIONS WHERE THE SURFACE PRESSURE IS LESS THAN 1000 OR
C      850 MB.  TROPOPAUSE LEVEL AND MAX WIND LEVEL ARE ALSO
C      IDENTIFIED.  POTENTIAL TEMPERATURE IS USED FOR P<700 MB
C      WHERE POSSIBLE
C-----
CCCCC
      INTEGER HEIGHT(100),PRESSURE(100),IFRAME(100),TEMP(100),DP(100)
      INTEGER NDIR(100),NSPD(100),PML(11)
      INTEGER IFR(2),IHR(2),IDY(2),IMO(2),IYR(2),F(11),ITS(11),
      .      ITSH(11)
      INTEGER IFR1(2),ID1(2),IBLK(2),IELE(2),IFLG(2)
      INTEGER H1000,H850,TROPL,IHYL,TRINDEX
      REAL LAT,LON
CCCCC*
      INTEGER II,ICOUNT,ILAT,ILON,IFLAG,NUMPTS,NSND,MAXL,IERR,NWBAN,
      .      NKCT,IDUM2,IMW,INUM,I,IHY,IFR2,IC,IFR3,K,M,N,NML,NN,J,
      .      NHC,NTC,NTHC,NSC,NSDM,IR
      REAL   COUNT,TSP,SHP,CH

CCCCC+
      COMMON /ONE/ HEIGHT,PRESSURE,IFRAME,TEMP,DP
      COMMON /TWO/ NDIR,NSPD,I,NWBAN
      COMMON /THREE/ IFR,IHR,IDY,IMO,IYR
      COMMON /FOUR/ IFR1,ID1,IBLK,IELE
      COMMON /FIVE/ LAT,LON,NID,ICOUNT,ILAT,ILON,IFR2,NUMPTS
      COMMON /SIX/ IR,IC,IFR3,IFLAG,IHY,IMW,IDUM2,INUM
      COMMON /SEVEN/ NML,NHC,NTC,NTHC,NSC,J,NSDM

CCCCC
      DATA PML/1099,1000,850,700,500,400,300,250,200,150,100/

CCCCC
C==
      PRINT*,'PLEASE INPUT THE NAME OF INPUT FILE.  IFILE=? (A, <=32)'
      ACCEPT 'A',IFILE

      OPEN(UNIT=11,FILE='HYCHECK.OUT1',STATUS='NEW')
      OPEN(UNIT=13,FILE='HYCHECK.OUT2',STATUS='NEW')
C      OPEN(UNIT=11,FILE='WRP1:[SCHWARTZ]RAOB.OUTPUT',STATUS='NEW')
C      OPEN(UNIT=13,FILE='ESG_SCRATCH:[SCHWARTZ]RAOB.DT',STATUS='NEW')
C==
      OPEN(UNIT=12,FILE=IFILE,STATUS='OLD')

CCCCC
      DATA NML/0/,NHC/0/,NTC/0/,NTHC/0/,NSC/0/,NSDM/0/,NSND/0/
      DO 10 II=1,11
         ITS(II)=0
         ITSH(II)=0
10      CONTINUE
CCCCC
      READ A,KC,FORMATTED,SOUNDING
      ICOUNT=0
      ILAT=32767
      ILON=32767
      IFLAG=0
CCCCC
      CALL READKC()

```

[Page 1 of 38 pages of Code]